

# NAVAL POSTGRADUATE SCHOOL

## Monterey, California

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# THESIS

APPROXIMATE INTERVAL ESTIMATION  
METHODS FOR THE  
RELIABILITY OF SYSTEMS USING COMPONENT  
DATA WITH EXPONENTIAL  
AND WEIBULL DISTRIBUTIONS

by

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September, 1989

Thesis Advisor

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Unclassified

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## REPORT DOCUMENTATION PAGE

1a Report Security Classification <b>Unclassified</b>		1b Restrictive Markings	
2a Security Classification Authority		3 Distribution Availability of Report <b>Approved for public release; distribution is unlimited.</b>	
2b Declassification Downgrading Schedule			
4 Performing Organization Report Number(s)		5 Monitoring Organization Report Number(s)	
6a Name of Performing Organization <b>Naval Postgraduate School</b>	6b Office Symbol (if applicable) <b>55</b>	7a Name of Monitoring Organization <b>Naval Postgraduate School</b>	
6c Address (city, state, and ZIP code) <b>Monterey, CA 93943-5000</b>		7b Address (city, state, and ZIP code) <b>Monterey, CA 93943-5000</b>	
8a Name of Funding Sponsoring Organization	8b Office Symbol (if applicable)	9 Procurement Instrument Identification Number	
8c Address (city, state, and ZIP code)		10 Source of Funding Numbers Program Element No   Project No   Task No   Work Unit Accession No	
11 Title (Include security classification) <b>APPROXIMATE INTERVAL ESTIMATION METHODS FOR THE RELIABILITY OF SYSTEMS USING COMPONENT DATA WITH EXPONENTIAL AND WEIBULL DISTRIBUTIONS</b>			
12 Personal Author(s) <b>LEE, Hyeon-Soo</b>			
13a Type of Report <b>Master's Thesis</b>	13b Time Covered From To	14 Date of Report (year, month, day) <b>September, 1989</b>	15 Page Count <b>64</b>
16 Supplementary Notation <b>The views expressed in this thesis are those of the author and do not reflect the official policy or position of the Department of Defense or the U.S. Government.</b>			
17 Cosati Codes Field   Group   Subgroup		18 Subject Terms (continue on reverse if necessary and identify by block number) <b>Reliability, Jackknife, Confidence Limit, Exponential, Weibull, <del>Normal</del> Newton - Raphson,</b>	
19 Abstract (continue on reverse if necessary and identify by block number) → Two approximate parametric interval estimation methods for system reliability using component test data are developed and evaluated. One method can be applied to any coherent system with components which have <i>exponential</i> failure times with possibly different failure rates and different mission operating times. This method estimates the ratios of component failure rates which are then used to develop the approximate lower confidence limit. These ratio estimates are developed with and without jackknife methods and the two results are compared. This procedure is very accurate and simple to compute, requiring the use of standard chi-square tables. This <i>ratio</i> method is subsequently extended to coherent systems with components whose failure times have a <i>Weibull</i> distribution. A nearly exact parametric lower confidence limit for $P(X > x)$ is developed and evaluated where $x$ is given and $X$ has a <i>normal</i> distribution with unknown mean and variance. This procedure is also simple to evaluate and requires the use of <i>Student t</i> tables. <i>Keywords: theses,</i>			
20 Distribution Availability of Abstract <input checked="" type="checkbox"/> unclassified unlimited <input type="checkbox"/> same as report <input type="checkbox"/> DTIC users		21 Abstract Security Classification <b>Unclassified</b>	
22a Name of Responsible Individual <b>W.M. WOODS</b>		22b Telephone (Include Area code) <b>(408) 484-1893</b>	22c Office Symbol <b>55Wo</b>

DD FORM 1473, 84 MAR

83 APR edition may be used until exhausted  
All other editions are obsolete

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Approximate Interval Estimation Methods for the Reliability  
of Systems Using Component Data with Exponential and  
Weibull Distributions

by

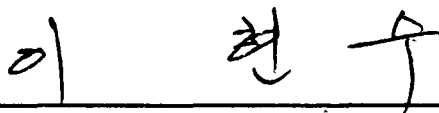
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Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

from the

NAVAL POSTGRADUATE SCHOOL  
September, 1989



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## ABSTRACT

Two approximate parametric interval estimation methods for system reliability using component test data are developed and evaluated. One method can be applied to any coherent system with components which have *exponential* failure times with possibly different failure rates and different mission operating times. This method estimates the ratios of component failure rates which are then used to develop the approximate lower confidence limit. These ratio estimates are developed with and without jackknife methods and the two results are compared. This procedure is very accurate and simple to compute, requiring the use of standard chi-square tables. This *ratio* method is subsequently extended to coherent systems with components whose failure times have a *Weibull* distribution. A nearly exact parametric lower confidence limit for  $P(X > x)$  is developed and evaluated where  $x$  is given and  $X$  has a *normal* distribution with unknown mean and variance. This procedure is also simple to evaluate and requires the use of *Student t* tables.

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DTIC TAB	<input type="checkbox"/>
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<b>Availability Codes</b>	
Dist	Avail and/or Special
A-1	



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## I. BACKGROUND

Parametric confidence interval procedures for the reliability of mechanical systems are much less developed than procedures for electrical systems. This is due to the more complicated failure distributions used to model mechanical hardware. The failure rate of a *series* system of independent components, with *exponentially* distributed failure times and equal mission times, is the sum of the failure component failure rates. This property has permitted development of numerous methods for system reliability of series and other coherent systems using component failure data. The *Weibull* and *extreme value* distributions have been used in life testing methods for both electrical and mechanical devices. Several methods have been used for obtaining point estimates of parameters for these distributions and for the reliability function itself, Harter and Moore [Ref. 1: pp. 889-901], Mann [Ref. 2: pp. 231-256].

The derivation of simple confidence limits for the reliability function for the *extreme value* distribution with parameters  $z$  and  $\delta$  has posed problems, because methods based on a pivotal quantity such as  $(\hat{z} - z)/\hat{\delta}$  are inadequate. Lawless [Ref. 3: pp. 355-364], Johns and Lieberman [Ref. 4: pp. 135-175] and Thoman, Bain and Antle [Ref. 5: pp. 363-372] have developed nearly exact procedures for confidence limits for the reliability function of the *Weibull* and *extreme value* distributions. Schneider and Weissfeld [Ref. 6: pp. 179-186] have developed interval estimation methods for percentiles of the *Weibull* and *extreme value* distribution based on censored data. Although extensive methods have been developed for interval estimates of the reliability of a single component with the *Weibull* or *extreme value* failure distribution, very few parametric interval methods have been developed for system reliability using component test data with *Weibull* failure distributions.

Two approximate parametric interval estimation methods for reliability of coherent systems using component test data are developed and evaluated in this thesis. Evaluations of these procedures are performed using computer simulation for series systems only. One of these methods is developed for the reliability of a series system whose components have *exponential* failure distributions and different mission times. This procedure was found to be quite accurate and can be applied to coherent systems in general. This first procedure is then extended to the case where components of the sys-



tem have *Weibull* failure distributions. The method used is an extension of a non-parametric method developed by Myhr, J., Rosenfeld, A. and Saunders, S. [Ref. 7: pp.213-227].

The *normal* distribution is used extensively in some mechanical reliability models. Maximum likelihood and minimum variance unbiased estimators for  $P(X \geq x_0)$  when both  $\mu$  and  $\sigma^2$  are unknown were developed over thirty years ago, Lieberman and Resnikoff [Ref. 8: pp. 457-516], Folks and others [Ref. 9: pp. 43-50], and Barton [Ref. 10: pp. 227-229]. Exact interval estimation procedures for  $P(X \geq x_0)$  were developed by Owen and Hua [Ref. 11: pp.285-311] using the non-central  $t$  distribution. Letting  $X$  denote strength and  $Y$  denote stress, mechanical reliability is sometimes modeled as the value for  $P(X > Y)$ . Approximate interval estimation procedures for this probability when  $X$  and  $Y$  are assumed to be normal have been developed by Church and Harris [Ref. 12: pp. 49-54] when the mean and variance of  $Y$  are known. Downton [Ref. 13: pp. 551-558] modifies their procedure slightly to get more accurate bounds and suggests an approximate procedure when the means and variances of both  $X$  and  $Y$  are unknown. Lower confidence intervals for  $P(X \geq Y)$  obtained under the assumption of normality for  $X$  and  $Y$  can lead to serious error when either  $X$  or  $Y$  or both are truncated well into the tails. Consequently,  $P(X \geq x_0)$  may be a more reasonable model of mechanical reliability where  $x_0$  is chosen conservatively. A very accurate approximate lower confidence limit procedure for  $P(X \geq x_0)$  is developed and evaluated in this thesis. It can be computed easily.

## II. INTERVAL ESTIMATION PROCEDURE - EXPONENTIAL CASE

A system of independent components is coherent if an increase in reliability of any one of its components does not cause a degradation in system reliability. Suppose a coherent system has  $k$  components. We assume that the failure distribution of component  $i$  is *exponential* with failure rate  $\lambda_i$ . Then system reliability  $R_S$  can be written as a function of  $\lambda_i, t_i, i = 1, 2, \dots, k$ ; i.e.,

$$R_S(t) = g(\lambda_1, \lambda_2, \dots, \lambda_k, t_1, t_2, \dots, t_k)$$

where  $t_i = t_i(t)$  is the operating time for component  $i, i = 1, 2, \dots, k$ .

Let  $\lambda_m = \max\{\lambda_1, \lambda_2, \dots, \lambda_k\}$  and  $r_i = \lambda_i/\lambda_m, i = 1, 2, \dots, k$ . Then one can write

$$R_S(t) = g(\lambda_m, r_1, \dots, r_k, t_1, \dots, t_k)$$

If the  $r_i$  were known and  $\hat{\lambda}_{m,U(\alpha)}$  were an upper  $100(1 - \alpha)\%$  confidence limit for  $\lambda_m$ , the corresponding lower confidence limit for  $R_S(t)$  would be

$$\hat{R}_S(t)_{L(\alpha)} = g(\hat{\lambda}_{m,U(\alpha)}, r_1, \dots, r_k, t_1, \dots, t_k)$$

Specifically, if the system is a *series* system of independent components, so that

$$R_S(t) = \exp\left\{-\sum_{i=1}^k \lambda_i t_i\right\} = \exp\left\{-\lambda_m \sum_{i=1}^k r_i t_i\right\} \quad (2.1)$$

then,

$$\hat{R}_S(t)_{L(\alpha)} = \exp\left\{-\hat{\lambda}_{m,U(\alpha)} \sum_{i=1}^k r_i t_i\right\}$$

If  $n_i$  items of component  $i$  are tested until failure,  $T_i$  denotes the total test time accumulated by all  $n_i$  items and  $n = \sum_{i=1}^k n_i$ , then  $2\lambda_m \sum_{i=1}^k r_i T_i$  is  $\chi^2_{2n}$ . See Bain and Engelhardt [Ref. 14].

An upper confidence limit for  $\lambda_m$  is

$$\hat{\lambda}_{m,U(\alpha)} = \frac{\chi_{\alpha, 2n}^2}{2 \sum_{l=1}^k r_l T_l} \quad (2.2)$$

where  $\chi_{\alpha, 2n}^2$  is the 100(1 -  $\alpha$ )th percentile of the  $\chi_n^2$  distribution. Corresponding equations for truncated testing are similar.

If the  $r_i$  are unknown, the following methods estimate the values for  $r_i$  from the data. One method uses the likelihood ratio estimate for  $r_i$ . The second method uses a jackknifed version of the first method. The two resulting confidence limits  $\hat{R}_{S,L(\alpha)}$  and  $R_{S,L(\alpha)}$ , with and without jackknifing  $\hat{r}_i$  respectively, are compared for relative accuracy. Quenouille [Ref. 15: pp. 353-360] first reported a method for estimating ratios that reduced the bias without increasing the variance. Miller [Ref. 16: pp. 1-15] gives an excellent review of the jackknife method which includes a discussion on the application of jackknifing to estimating ratios.

#### A. LOWER CONFIDENCE LIMIT $R_{S,L}$ WITHOUT JACKKNIFING

In this case, the maximum likelihood estimate of the ratio  $r_i = \frac{\hat{\lambda}_i}{\hat{\lambda}_m}$  is

$$\hat{r}_i = \frac{\hat{\lambda}_i}{\hat{\lambda}_m} \quad (2.3)$$

where  $\hat{\lambda}_i = n_i/T_i$  and  $\hat{\lambda}_m = \max(\hat{\lambda}_1, \dots, \hat{\lambda}_k)$ . The resulting approximate upper confidence limit for  $\lambda_m$  is

$$\hat{\lambda}_{m,U(\alpha)} = \frac{\chi_{\alpha, 2n}^2}{2 \sum_{l=1}^k \hat{r}_l T_l} \quad (2.4)$$

where  $n = \sum_{i=1}^k n_i$ , and

$$T_i = \sum_{j=1}^{n_i} T_{ij} \quad i = 1, 2, \dots, k \quad (2.5)$$

and  $T_{ij}$  denotes the failure time of the  $j$ th test for component  $i$ .

The resulting approximate confidence bound  $R_{S,L(\alpha)}$  is given by

$$R_{S,L(x)} = \exp \left\{ -\hat{\lambda}_{m,U(x)} \sum_{l=1}^k \hat{r}_l t_l \right\} \quad (2.6)$$

## B. LOWER CONFIDENCE LIMIT $\hat{R}_{S,L}$ WITH JACKKNIFING

The definitions for  $\hat{\lambda}_i$ ,  $\hat{r}_i$ ,  $n_i$ , and  $T_i$  in Section A are also used in this section. Let  $\hat{\lambda}_{ij(\bullet)}$  denote the estimate for  $\lambda_i$  by removing  $T_{ij}$  from the data ; i.e.,

$$\hat{\lambda}_{ij(\bullet)} = \frac{n_i - 1}{\sum_{l=1} T_{il}} \quad j = 1, 2, \dots, n_i, \quad l \neq j \quad (2.7)$$

and

$$\hat{\lambda}_{mj(\bullet)} = \frac{n_m - 1}{\sum_{l=1} T_{ml}} \quad j = 1, 2, \dots, n_m, \quad l \neq j \quad (2.8)$$

Then the jackknifed ratio estimate  $\hat{r}_i^*$  is given by

$$\hat{r}_i^* = n^* \hat{r}_i - \frac{(n^* - 1) \sum_{j=1}^{n^*} \hat{r}_{ij(\bullet)}}{n^*} \quad (2.9)$$

where  $n^* = \min(n_1, n_2, \dots, n_k)$  and

$$\hat{r}_{ij(\bullet)} = \frac{\hat{\lambda}_{ij(\bullet)}}{\hat{\lambda}_{mj(\bullet)}} \quad j = 1, 2, \dots, n^* \quad (2.10)$$

Now define  $\hat{\lambda}_{U(x)}^*$  by

$$\hat{\lambda}_{U(x)}^* = \frac{\chi_{\alpha, 2n}^2}{2 \sum_{l=1}^k \hat{r}_l^* T_l}, \quad (2.11)$$

The corresponding confidence bound  $\hat{R}_{S,L(x)}$  is given by

$$\hat{R}_{S,L(\alpha)} = \exp \left\{ - \hat{\lambda}_{U(\alpha)}^* \sum_{i=1}^k \hat{r}_i^* t_i \right\} \quad (2.12)$$

When the  $n_i$ ,  $i = 1, 2, \dots, k$  differ considerably, this jackknife estimation procedure can be unbalanced. That is, the number of data points used to compute the jackknife estimate will differ from one component to another. It was decided to use this jackknifing procedure and determine the effect of differing sample sizes by examining the results of the simulations.

In equation (2.9), the jackknife estimate is constructed by using only the first  $n^*$  observations from each component to obtain  $\hat{r}_{ij(n^*)}$ , where  $n^* = \min\{n_1, n_2, \dots, n_k\}$ . Of course it is rather arbitrary to take the first  $n^*$  observations from  $n_i$ , since any  $n^*$  of the collection of  $n_i$  values could be used.

### C. SIMULATIONS AND RESULTS FOR EXPONENTIAL CASE

#### 1. Simulation

##### a. Simulation language and package

The programming language used to simulate this problem was VS FORTRAN on an IBM 3033. Also LEXPN in LLRANII was used to generate observed exponential random variates. SHSORT was used to perform the sort routines.

##### b. Cases and Input parameters

The six input parameters below determine the conditions for exercising the simulation runs. System reliability is determined by five parameters. Values of these parameters are given in the tables that show the results. The test plan simulated was to test  $n_i$  items until all fail.

- number of component types,  $k$  : 5 and 15
- system reliability,  $R_s$  : 0.9 and 0.975
- significance level,  $\alpha$  : 0.05 and 0.2
- component time,  $t_i$  : small to large (see tables)
- sample size,  $n_i$  : small to large (see tables)

Reliability of a *series* system is expressed as  $R_s = \exp\{-\sum_{i=1}^k \lambda_i t_i\}$ . We chose arbitrarily to determine the failure rates,  $\lambda_i$ , from this equation by assuming all  $\lambda_i t_i$  to be equal, consequently,

$$\lambda_i = \frac{-\ln R_S}{k t_i} .$$

### c. Replications

The procedure was replicated 1000 times for each case to get 1000 values of  $R_{S,L(s)}$  and 1000 values of  $\hat{R}_{S,L(s)}$ . We order each set of the 1000 values of  $R_{S,L(s)}$  and  $\hat{R}_{S,L(s)}$  in ascending order. Then the two approximate confidence bounds,  $R_{S,L(s)(100(1-\alpha))}$  and  $\hat{R}_{S,L(s)(100(1-\alpha))}$ , for  $R_S$  are the 1000(1 -  $\alpha$ )th order values of these two sets of data. Finally, for each of the two ordered sets of data, we find the order indices  $j_1$  and  $j_2$  for which  $R_{S,L(s)(j_1)}$  and  $\hat{R}_{S,L(s)(j_2)}$  are closest to  $R_S$  for their respective sets. Then  $j_1 / 1000$  and  $j_2 / 1000$  are called the two corresponding simulated true confidence levels.

## 2. Results

Tables 1 through 3 show the results of the 3 cases simulated. The results indicate that this interval estimation method using estimates of failure rate ratios will yield quite accurate lower confidence limits for system reliability when components have unknown constant failure rates. The jackknife method also yields very accurate confidence limits which are slightly conservative. That is the 100(1 -  $\alpha$ ) percentile points of  $\hat{R}_{S,L(s)}$ , given in the tables, are slightly less than the true value of  $\hat{R}_S$ . Consequently,  $P(\hat{R}_{S,L(s)} \leq R_S) > 1 - \alpha$ . Alternatively, one can say  $\hat{R}_{S,L(s)}$  is a conservative 100(1 -  $\alpha$ ) percent lower confidence limit procedure for  $R_S$ .

**Table 1. RELIABILITY OF A SERIES SYSTEM WITH SMALL NUMBER  
( LESS THAN 10 ) OF SAMPLE SIZES - EXPONENTIAL CASE**

Number of Compo- nents	Reliability of System	$\alpha$	Lower Confidence Limit		True Confidence Limit	
			W/O Jackknifing	WITH Jackknifing	W/O Jackknifing	WITH Jackknifing
5	.90	.2	0.9017	0.8904	0.7720	0.9100
		.05	0.8985	0.8889	0.9620	0.9780
	.975	.2	0.9750	0.9720	0.8020	0.9160
		.05	0.9746	0.9729	0.9600	0.9800
15	.90	.2	0.9019	0.8901	0.7600	0.9500
		.05	0.9012	0.8933	0.9300	0.9800
	.975	.2	0.9745	0.9724	0.8300	0.9600
		.05	0.9746	0.9725	0.9600	0.9800

Sample sizes for 5 components are 9, 7, 10, 8, 6

Sample sizes for 15 components are 6, 7, 5, 6, 7, 8, 9, 5, 8, 7, 9, 10, 7, 9, 6

Component times  $t_i$  are 2, 3, 7, 8, 10, 3, 7, 10, 1, 7, 8, 3, 10, 1, 8

**Table 2. RELIABILITY OF A SERIES SYSTEM WITH MEDIUM NUMBER  
( LESS THAN 30 ) OF SAMPLE SIZES - EXPONENTIAL CASE**

Number of Compo- nents	Reliability of System	$\alpha$	Lower Confidence Limit		True Confidence Limit	
			W/O Jackknifing	WITH Jackknifing	W/O Jackknifing	WITH Jackknifing
5	.90	.2	0.8999	0.8978	0.8020	0.8660
		.05	0.8990	0.8983	0.9600	0.9680
	.975	.2	0.9750	0.9745	0.8000	0.8460
		.05	0.9748	0.9745	0.9620	0.9740
15	.90	.2	0.8992	0.8960	0.8300	0.9100
		.05	0.8980	0.8981	0.9600	0.9700
	.975	.2	0.9751	0.9738	0.7900	0.9000
		.05	0.9750	0.9741	0.9500	0.9800

Sample sizes for 5 components are 30, 21, 10, 15, 26

Sample sizes for 15 components are 3, 7, 10, 15, 20, 15, 7, 5, 30, 20, 10, 7, 13, 21, 30

**Table 3. RELIABILITY OF A SERIES SYSTEM WITH LARGE NUMBER  
( LESS THAN 100 ) OF SAMPLE SIZES - EXPONENTIAL CASE**

Number of Compo- nents	Reliability of System	$\alpha$	Lower Confidence Limit		True Confidence Limit	
			W/O Jackknifing	WITH Jackknifing	W/O Jackknifing	WITH Jackknifing
5	.90	.2	0.8999	0.8991	0.8080	0.8200
		.05	0.8990	0.8992	0.9680	0.9620
	.975	.2	0.9750	0.9750	0.8540	0.8060
		.05	0.9751	0.9750	0.9380	0.9520
15	.90	.2	0.9000	0.8988	0.8010	0.8750
		.05	0.9000	0.8996	0.9500	0.9590
	.975	.2	0.9750	0.9747	0.8460	0.8730
		.05	0.9750	0.9750	0.9520	0.9470

Sample sizes for 5 components are 30, 63, 75, 98, 26

Sample sizes for 15 components are 15, 40, 35, 17, 26, 67, 50, 65, 80, 32, 95, 100, 15, 45, 30



### III. INTERVAL ESTIMATION PROCEDURE - WEIBULL CASE

#### A. LOWER CONFIDENCE LIMIT $R_{S,L}$

Consider a *series* system with  $k$  components. Let the time to failure  $X_i$  of component  $i$  have a *Weibull* distribution with density

$$f_i(t_i) = \lambda_i^{\beta_i} \beta_i t_i^{\beta_i-1} \exp\{-(\lambda_i t_i)^{\beta_i}\}, \quad t_i > 0. \quad (3.1)$$

Then

$$R_i(t_i) = \exp\{-(\lambda_i t_i)^{\beta_i}\}, \quad t_i > 0 \quad (3.2)$$

and

$$R_S(t) = \exp\left\{-\sum_{i=1}^k \lambda_i^{\beta_i} t_i^{\beta_i}\right\} = \exp\left\{-\lambda_m^* \sum_{i=1}^k r_i t_i^{\beta_i}\right\}, \quad t > 0. \quad (3.3)$$

where  $\lambda_i^* = \lambda_i^{\beta_i}$ ,  $\lambda_m^* = \max_i \lambda_i^*$  and  $r_i = \lambda_i^*/\lambda_m^*$ . If the  $\beta_i$  are known,  $X_i^{\beta_i}$  has constant failure rate  $\lambda_i^{\beta_i}$  and the procedures in Chapter II can be used to obtain  $\hat{R}_{S,L(a)}$  and  $R_{S,L(a)}$  with  $T_y$  replaced by  $T_y^{\beta_i}$  in equation (2.5). It is well known that  $Y \equiv \ln X_i$  has an *extreme value* distribution with CDF

$$F_Y(y) = 1 - \exp\left\{-e^{\frac{y-\xi}{\delta_i}}\right\}$$

where  $\xi_i = \ln(1/\lambda_i)$  and  $\delta_i = 1/\beta_i$ .

Engelhardt and Bain [Ref. 17: p. 323] have developed the following simple unbiased estimators for  $\xi_i$  and  $\delta_i$ , using ordered values  $Y_{(j)} = \ln X_{(j)}$

$$\hat{\delta}_i = \frac{1}{\hat{\beta}_i} = \frac{-\sum_{j=1}^s Y_{(j)} + \frac{s}{n-s} \sum_{j=s+1}^n Y_{(j)}}{n_i k_{n_i}} \quad (3.4)$$

where  $s = [0.84n_i] \equiv \text{largest integer} \leq 0.84 n_i$  and  $X_{(j)}$  is the  $j$ th order statistics from the sample of size  $n_i$  of  $X_i$ . Also

$$\hat{\xi}_i = \ln\left(\frac{1}{\hat{\lambda}}\right) = \bar{y}_i + \gamma \hat{\delta} \quad (3.5)$$

where  $\gamma = 0.5772$  and  $\bar{y}_i = \sum_{j=1}^{n_i} Y_{ij}/n_i$ . Let

$$\hat{\beta}_i = \frac{1}{\hat{\delta}_i} \quad (3.6)$$

and

$$T_{ij} = X_{ij}^{\hat{\beta}_i} \quad i = 1, 2, \dots, n_i \quad j = 1, 2, \dots, k. \quad (3.7)$$

We approximate the distribution of  $T_{ij}$  by the *exponential* distribution with failure rate  $\hat{\lambda}_i^{\hat{\beta}_i} \equiv \hat{\lambda}_i^*$  and proceed as in Chapter II. Define

$$\hat{\lambda}_i^* = \frac{n_i}{T_i} \quad (3.8)$$

where  $T_i = \sum_{j=1}^{n_i} T_{ij}$   $i = 1, 2, \dots, k$ . Let  $\hat{\lambda}_m^* = \max_i \hat{\lambda}_i^*$  and

$$\hat{r}_i = \frac{\hat{\lambda}_i^*}{\hat{\lambda}_m^*} \quad (3.9)$$

Then an approximate upper confidence limit for  $\hat{\lambda}_m^*$  is given by

$$\hat{\lambda}_{m,U(x)}^* = \frac{\chi_{\alpha, 2n}^2}{2 \sum_{i=1}^k \hat{r}_i T_i} \quad (3.10)$$

and the corresponding approximate lower confidence limit  $R_{S,L(x)}$  for  $R_S(t)$  is given by

$$R_{S,L(x)} = \exp\left\{-\hat{\lambda}_{m,U(x)}^* \sum_{i=1}^k \hat{r}_i t_i^{\hat{\beta}_i}\right\} \quad (3.11)$$

where  $n = \sum_{i=1}^k n_i$ .

This procedure is labeled the Formula procedure in the tables that follow in this section. Its distinguishing feature is the equation for  $\hat{\beta}_i$  given by equation (3.6). An alternative procedure, labeled the Newton - Raphson procedure, estimates  $\beta_i$  using the

maximum likelihood procedure which is obtained using a Newton - Raphson approximation method. Equations for  $\hat{\beta}_i$  under the Newton - Raphson procedure are provided in Appendix A.

## B. SIMULATIONS AND RESULTS

### 1. Simulation

#### a. Simulation language and package

The programming language used to simulate this problem was VS FORTRAN on an IBM 3033. Also LEXPN in LLRANII was used to generate observed exponential random variates. SHSORT was used to perform the sort routines.

#### b. Cases and Input parameters

The six input parameters below determine the conditions for exercising the simulation runs. System reliability is determined by five parameters. Values of these parameters are given in the tables that show the results. The test plan simulated was to test  $n_i$  items until all fail.

- number of component types,  $k$  : 5 and 15
- system reliability,  $R_S$  : 0.9 and 0.975
- significance level,  $\alpha$  : 0.05 and 0.2
- component time,  $t_i$  : small to large (see tables)
- sample size,  $n_i$  : small to large (see tables)

Reliability of a *series* system is expressed as  $R_S = \exp\{-\sum_{i=1}^k \lambda_i t_i\}$ . Failure rates  $\lambda_i$  can be determined from that equation by assuming all  $\lambda_i t_i$  to be equal, consequently,

$$\lambda_i = \frac{-\ln R_S}{k t_i}.$$

#### c. Replications

The procedure was replicated 1000 times for each case to get 1000 values of  $R_{S,L(\alpha)}$  and 1000 values of  $\hat{R}_{S,L(\alpha)}$ . We order each set of the 1000 values of  $R_{S,L(\alpha)}$  and  $\hat{R}_{S,L(\alpha)}$  in ascending order. Then the two approximate confidence bounds,  $R_{S,L(\alpha)(1000(1-\alpha))}$  and  $\hat{R}_{S,L(\alpha)(1000(1-\alpha))}$ , for  $R_S$  are the 1000(1 -  $\alpha$ )th order values of these two sets of data. Finally, for each of the two ordered sets of data, we find the order indices  $j_1$  and  $j_2$  for which  $R_{S,L(\alpha)(j_1)}$  and  $\hat{R}_{S,L(\alpha)(j_2)}$  are the closest to  $R_S$  for their respective sets. Then  $j_1 / 1000$  and  $j_2 / 1000$  are called the two corresponding true confidence levels.

## 2. Results

Tables 4 and 5 display the results of the simulations and determine the accuracy of  $\hat{R}_{S,L(\alpha)}$  given in equation (3.11) as a lower confidence limit procedure for system reliability,  $R_S$ , for parameter values  $\lambda$ ,  $\beta$ ,  $t$ , and  $R_S$  given in the tables. The terms in the tables have the same meaning as the corresponding terms in Tables 1 through 3 which were explained in Section 2.C.2. The procedure would be exact for the Formula method if the values in the Formula column equal the corresponding numbers in the same row in the Reliability of System column. In Table 4 for example, the 80th percentile point of .9205 for the Newton - Raphson procedure is more accurate than the Formula procedure which has an 80th percentile point of .9324. The last column shows, however, that what we have called an 80% lower confidence limit procedure is in fact closer to a 61% procedure. The accuracy improves if the sample size is increased from 15 to 30 as indicated in Table 5. The accuracy improves even more if the number of components in the system increases from 5 to 15 as indicated in Tables 4 and 5.

The results in Tables 4 and 5 show that the  $\hat{R}_{L(\alpha)}$  method given by equation (3.11) is too optimistic - especially for small sample sizes and for systems with a small number of components. Modifications to this procedure are needed. These tables also indicate that the Newton - Raphson method is superior to the Formula method.

**Table 4. ACCURACY OF  $R_{s,L}$  AS A LOWER CONFIDENCE LIMIT FOR  $R_s$  WITH SAMPLE SIZES OF 15 - WEIBULL CASE**

Number of Components	Reliability of System	$\alpha$	Lower Confidence Limit		True Confidence Limit	
			Formula	Newton Raphson	Formula	Newton Raphson
5	.90	.2	0.9324	0.9205	0.4820	0.6060
		.05	0.9512	0.9406	0.5380	0.6660
	.975	.2	0.9849	0.9824	0.5040	0.6540
		.05	0.9905	0.9891	0.5600	0.6660
15	.90	.2	0.9193	0.9030	0.5440	0.7620
		.05	0.9416	0.9288	0.6060	0.7760
	.975	.2	0.9802	0.9747	0.6160	0.8080
		.05	0.9865	0.9828	0.6580	0.8240

Initial beta for 5 components are 2.2, 2.4, 2.6, 2.8, 2.5

Initial beta for 15 components are 2.2, 2.4, 2.6, 2.8, 2.5, 2.3, 2.7, 2.5, 2.2, 2.6, 2.9, 2.8, 2.4, 2.6, 2.1

Component times  $t_i$  are 2, 3, 7, 8, 10, 3, 7, 10, 1, 7, 8, 3, 10, 1, 8

**Table 5. ACCURACY OF  $R_{s,L}$  AS A LOWER CONFIDENCE LIMIT FOR  $R_s$  WITH SAMPLE SIZES OF 30 - WEIBULL CASE**

Number of Components	Reliability of System	$\alpha$	Lower Confidence Limit		True Confidence Limit	
			Formula	Newton Raphson	Formula	Newton Raphson
5	.90	.2	0.9249	0.9125	0.4100	0.6320
		.05	0.9424	0.9321	0.5100	0.6940
	.975	.2	0.9837	0.9798	0.4380	0.6160
		.05	0.9879	0.9845	0.4600	0.6760
15	.90	.2	0.9207	0.9036	0.5560	0.7200
		.05	0.9333	0.9198	0.4380	0.7520
	.975	.2	0.9808	0.9758	0.5120	0.7520
		.05	0.9850	0.9810	0.5200	0.7920

Initial beta for 5 components are 2.2, 2.4, 2.6, 2.8, 2.5

Initial beta for 15 components are 2.2, 2.4, 2.6, 2.8, 2.5, 2.3, 2.7, 2.5, 2.2, 2.6, 2.9, 2.8, 2.4, 2.6, 2.1

## IV. INTERVAL ESTIMATION PROCEDURE - NORMAL CASE

### A. BACKGROUND

In recent years it has become popular to model mechanical reliability as  $P(X > Y)$  where  $X$  denotes strength and  $Y$  denotes stress. This formulation of reliability is an average of  $P(X > y | Y = y)$ , since

$$P(X > Y) = E_Y P(X > y) = \int P(X > y) f_Y(y) dy \quad ,$$

An alternative model is the worst case approach. In the worst case model, one selects a worst case value of  $y$ , say  $y_o$ , and then designs the strength,  $X$ , of the component so that  $P(X > y_o) = R_o$  where  $R_o$  is a reliability requirement. If  $X$  has a *normal* distribution then this requirement imposes constraints on the mean and variance of  $X$ . This is usually done in a manner to comply with standard "safety factor" procedures.

The average model,  $P(X > Y)$ , uses two random variables and is subject to more random error than the worst case model. The accuracy of the expression  $P(X > Y)$  for values of this expression close to one is highly suspect due to deviations in the tail probabilities of both  $X$  and  $Y$  from those assumed in the model. It is common to assume that both  $X$  and  $Y$  have normal distributions. *Truncated normal* distributions would be more appropriate for many types of mechanical equipment. Harris and Soms [Ref. 18: pp. 650-663] discuss implications of this problem. Very significant errors in point and interval estimation for reliability are readily demonstrated when  $X$  is *truncated normal* but assumed to be *normal* in the more simple model which specifies that  $R = P(X > Y)$ . Table 10 shows this effect when  $X$  is truncated above at  $\mu + 1.645\sigma$ , where  $Z_\alpha$  is the 100  $(1 - \alpha)$ th percentile point of the *standard normal* distribution. Church and Harris [Ref. 12: pp. 49-54] and Downton [Ref. 13: pp. 551-558] have developed approximate confidence intervals for  $P(X > Y)$  when  $X$  is *normal* with unknown mean and variance and  $Y$  has the *standard normal* distribution.

## B. EXACT AND APPROXIMATE INTERVAL ESTIMATES

Minimum variance unbiased estimators (MVUE) for  $R = P(X > y)$  are well known when  $X$  is *normal* with unknown mean and known variance and also when the variance is unknown. In the former case, Lieberman and Resnikoff [Ref. 8] developed the result

$$\hat{R} = \Phi\left(\frac{\bar{X} - y}{\sigma\sqrt{\frac{n-1}{n}}}\right)$$

which is MVUE for  $R$  where  $\Phi$  is the *standard normal* cumulative distribution function. When the variance is unknown, several versions of an integral expression for  $P(X > y)$  have been developed by Lieberman and Resnikoff [Ref. 8], Basu [Ref. 19] and Folks and others [Ref. 9].

Exact lower confidence interval estimates for  $P(X > y)$  when  $X$  is *normal* with unknown mean and variance involve the non-central  $t$  - distribution. Owen and Hua [Ref. 11] developed tables of the lower 90% and 95% confidence limit values  $R_L$  for  $P(X > y)$  based on the non-central  $t$  - distribution. These values are tabled for values of  $k$  in the range  $-3.0$  (.2)  $6.0$  and sample sizes  $n = 2$  (1)  $18$ ,  $21$  (3)  $30$ ,  $40$  (20)  $100$ , where  $k = (\bar{x} - y)/s$  and  $\bar{x}$  and  $s$  are the sample mean and standard deviation. Their tables are essentially exact. An approximation to their exact tabled values is given by  $R_L^*$  where  $R_L^* \equiv \Phi(\gamma^*)$ ,

$$\gamma^* = k - \left\{ \frac{1}{n} + \frac{k^2}{2(n - \sqrt{k})} \right\}^{\frac{1}{2}} t_{\alpha, n-1} \quad , \quad (4.1)$$

$k = (\bar{x} - y)/s$  and  $t_{\alpha, n-1}$  is the  $100(1 - \alpha)$ th percentile of the  $t$  distribution with  $n - 1$  degrees of freedom. Equation (4.1) was developed in this thesis. It is an extensive ad hoc modification of an equation developed by Church and Harris [Ref. 12]. Tables 6 and 7 display values of  $R_L \equiv \Phi(\gamma)$ ,  $\gamma$ ,  $\gamma^*$ ,  $R_L^*$ , and  $R_L^* - R_L$  for  $k = 1, 2, 3, 4$ , sample sizes  $n = 10, 18, 30$  and confidence levels 90% and 95%.  $R_L$  and  $\gamma$  denote the "exact" lower confidence limits and corresponding  $\Phi^{-1}(R_L)$  values from Owen and Hua [Ref. 11]. Both  $\gamma^*$  and  $R_L^*$  are given by equation (4.1). The accuracy of the approximate confidence interval is quite good relative to the values for  $R_L$  given by Owen and Hua [Ref. 11].

Table 6. APPROXIMATE (  $R_L^*$  ) AND EXACT (  $R_L$  ) 90% CONFIDENCE LIMITS FOR  $P(X > Y_0)$

n	$t_{.10, n-1}$	k	$R_L: \Phi(\gamma)$	$\gamma$	$\gamma^*$	$R_L^*: \Phi(\gamma^*)$	$R_L^* - R_L$
10	1.3830	1	0.68156	0.47194	0.45454	0.67528	-0.00628
		2	0.89130	1.23397	1.20199	0.88517	-0.00613
		3	0.97453	1.95262	1.88991	0.97025	-0.00428
		4	0.99602	2.65302	2.54950	0.99437	-0.00165
18	1.3334	1	0.73037	0.61385	0.61133	0.72950	-0.00087
		2	0.92569	1.44512	1.44038	0.92488	-0.00081
		3	0.98755	2.24314	2.23150	0.98684	-0.00071
		4	0.99877	3.02679	3.00614	0.99859	-0.00018
30	1.3114	1	0.75937	0.70424	0.70508	0.75960	0.00023
		2	0.94256	1.57740	1.57852	0.94248	-0.00008
		3	0.99233	2.42404	2.42459	0.99205	-0.00028
		4	0.99945	3.26207	3.25926	0.99940	-0.00005

Table 7. APPROXIMATE (  $R_L^*$  ) AND EXACT (  $R_L$  ) 95% CONFIDENCE LIMITS FOR  $P(X > Y_0)$

n	$t_{.05, n-1}$	k	$R_L: \Phi(\gamma)$	$\gamma$	$\gamma^*$	$R_L^*: \Phi(\gamma^*)$	$R_L^* - R_L$
10	1.8331	1	0.63052	0.33311	0.27702	0.60912	-0.02140
		2	0.85187	1.04477	0.94228	0.82692	-0.02495
		3	0.95565	1.70308	1.52864	0.93655	-0.01910
		4	0.99031	2.33813	2.07743	0.98075	-0.00956
18	1.7396	1	0.69504	0.51007	0.49292	0.68896	-0.00608
		2	0.90348	1.30221	1.26991	0.89777	-0.00571
		3	0.97996	2.05344	1.99739	0.97674	-0.00322
		4	0.99735	2.78717	2.70338	0.99638	-0.00097
30	1.6991	1	0.73361	0.62369	0.61789	0.73167	-0.00194
		2	0.92855	1.46579	1.45391	0.92677	-0.00178
		3	0.98855	2.27522	2.25448	0.98758	-0.00097
		4	0.99894	3.07140	3.04028	0.99873	-0.00021



Tables 8 and 9 display the results of computer simulations with 1,000 replications to check the accuracy of the  $R_L^*$  method for 80% and 90% lower confidence limits for  $P(X > y) \equiv R$  for  $y = 3$ , with various values of  $\sigma$  and  $\mu$  determined so that  $R$  equals the values shown. The procedure would be exact at the 80% level if the values in the column labelled  $\alpha = .2$  equal the corresponding values of  $R$  in the same row. The "true" confidence level corresponds to the index  $i(R)$  of 1,000 ordered values of  $R_{L(\alpha)}^*$  for which  $R_{L(\alpha), i(R)}^* = R$ . For example, in the seventh row of Table 8,  $R = .950$ ,  $\sigma_x = 20$ ,  $N = 10$ ,  $R_{L(.20), 800}^*$  was .9575, and  $R_{L(.10), 900}^*$  was .9533. Also  $R_{L(.20), 758}^* = .950$  and  $R_{L(.10), 886}^* = .950$ . Tables 8 and 9 indicate that the  $R_L^*$  procedure given by equation (4.1) is quite accurate at the 80% level of confidence for the cases simulated.

Table 8. ACCURACY ANALYSIS OF  $R_L^*$  PROCEDURE FOR 80% AND 90% LOWER CONFIDENCE LIMITS FOR  $P(X > 3)$  WHEN X IS NORMALLY DISTRIBUTED

R	$\sigma_x$	n	$R_{L,1000(1-\alpha)}$		True Confidence Level	
			$\alpha = .2$	$\alpha = .1$	$\alpha = .2$	$\alpha = .1$
.950	0.5	10	0.9624	0.9504	0.7310	0.8970
		25	0.9546	0.9542	0.7560	0.8820
		75	0.9517	0.9501	0.7800	0.8980
	1.0	10	0.9606	0.9531	0.7470	0.8910
		25	0.9501	0.9552	0.7970	0.8770
		75	0.9509	0.9528	0.7900	0.8770
	20.0	10	0.9575	0.9533	0.7580	0.8860
		25	0.9558	0.9551	0.7410	0.8730
		75	0.9511	0.9511	0.7830	0.8820
.990	0.5	10	0.9924	0.9913	1.0000	0.8840
		25	0.9906	0.9898	0.7800	0.9070
		75	0.9903	0.9907	0.9800	0.8780
	1.0	10	0.9921	0.9899	0.9990	0.9000
		25	0.9913	0.9904	0.7570	0.8910
		75	0.9904	0.9898	0.7800	0.9060
	20.0	10	0.9923	0.9922	0.9880	0.8750
		25	0.9909	0.9908	0.7760	0.8800
		75	0.9902	0.9903	0.7940	0.8920
.995	0.5	10	0.9966	0.9948	1.0000	0.9030
		25	0.9955	0.9949	0.7790	0.9020
		75	0.9956	0.9949	0.7540	0.9060
	1.0	10	0.9966	0.9952	1.0000	0.8950
		25	0.9960	0.9955	0.8630	0.8880
		75	0.9949	0.9947	0.8040	0.9150
	20.0	10	0.9970	0.9951	1.0000	1.0000
		25	0.9960	0.9957	0.7720	0.8700
		75	0.9951	0.9948	0.7940	0.9140

Table 9. ACCURACY ANALYSIS OF  $R_L^*$  PROCEDURE FOR 80% AND 90% LOWER CONFIDENCE LIMITS FOR  $P(X > 30)$  WHEN X IS NORMALLY DISTRIBUTED

R	$\sigma_x$	n	$R_{L,1000(1-\alpha)}$		True Confidence Level	
			$\alpha = .2$	$\alpha = .1$	$\alpha = .2$	$\alpha = .1$
.950	0.5	10	0.9621	0.9466	0.7510	0.9000
		25	0.9530	0.9519	0.7680	0.8890
		75	0.9507	0.9491	0.7880	0.9070
	1.0	10	0.9605	0.9528	0.7480	0.8910
		25	0.9497	0.9549	0.8030	0.8810
		75	0.9509	0.9527	0.7910	0.8780
	20.0	10	0.9575	0.9533	0.7580	0.8860
		25	0.9558	0.9551	0.7410	0.8730
		75	0.9511	0.9511	0.7830	0.8820
.990	0.5	10	0.9923	0.9911	1.0000	0.8860
		25	0.9900	0.9890	0.7990	0.9140
		75	0.9901	0.9904	0.7980	0.8860
	1.0	10	0.9921	0.9899	0.9990	0.9310
		25	0.9911	0.9902	0.7620	0.8950
		75	0.9904	0.9898	0.7800	0.9070
	20.0	10	0.9923	0.9922	0.9880	0.8750
		25	0.9909	0.9908	0.7760	0.8800
		75	0.9902	0.9903	0.7940	0.8840
.995	0.5	10	0.9965	0.9946	1.0000	0.9040
		25	0.9952	0.9946	0.7900	0.9140
		75	0.9955	0.9948	0.7620	0.9100
	1.0	10	0.9966	0.9951	1.0000	0.9280
		25	0.9959	0.9953	0.7610	0.8920
		75	0.9949	0.9947	0.8040	0.9140
	20.0	10	0.9970	0.9951	1.0000	1.0000
		25	0.9960	0.9957	0.7600	0.8700
		75	0.9951	0.9948	0.7940	0.9340

Table 10 displays the inaccuracies of the  $R_L^*$  lower confidence limit procedure for  $P(X > 3)$  using equation (4.1), which assumes  $X$  is  $N(\mu, \sigma^2)$ , when in fact  $X$  has the distribution of a *normal* random variable with mean  $\mu$  and variance  $\sigma^2$  that has been truncated at  $\mu + 1.645\sigma$ . Note that  $\mu + 1.645\sigma > 3$ , because  $P(X > 3) = .95, .99$  and  $.995$ .

Examination of Table 10 reveals gross inaccuracies; consequently, even when the distribution of  $X$  is truncated far above the value  $y$ , the exact lower confidence limit for  $P(X > y)$  can be greatly in error when computed under the assumption that  $X$  is *normal*. This problem will be compounded when one is computing "exact" confidence intervals for  $P(X > Y)$  assuming both  $X$  and  $Y$  are *normal* when in fact one or both may be *truncated normal*. This suggests that modeling mechanical reliability as  $P(X > Y)$  may be more risky than more standard engineering approaches for modeling mechanical reliability which include the notion of safety factors.

Table 10. ACCURACY ANALYSIS OF  $R_L^*$  PROCEDURE FOR 80% AND 90% LOWER CONFIDENCE LIMITS FOR  $P(X > 3)$  WHEN X IS TRUNCATED NORMAL

Reliability of System	$\sigma_x$	n	$R_{L,1000(1-\alpha)}$		True Confidence Level	
			$\alpha = .2$	$\alpha = .1$	$\alpha = .2$	$\alpha = .1$
.950	0.5	10	0.9806	0.0566	1.0000	1.0000
		25	0.8941	0.0125	1.0000	1.0000
		75	0.9383	0.0871	1.0000	1.0000
	1.0	10	0.8904	0.0419	1.0000	1.0000
		25	0.9555	0.0813	1.0000	1.0000
		75	0.9431	0.0782	1.0000	1.0000
	20.0	10	0.8503	0.0105	1.0000	1.0000
		25	0.9274	0.0485	1.0000	1.0000
		75	0.9496	0.1222	1.0000	1.0000
.990	0.5	10	0.9734	0.6035	1.0000	1.0000
		25	0.9924	0.6346	1.0000	1.0000
		75	0.9780	0.6552	1.0000	1.0000
	1.0	10	0.9976	0.9172	1.0000	1.0000
		25	0.9884	0.7505	1.0000	1.0000
		75	0.9951	0.6800	1.0000	1.0000
	20.0	10	0.9593	0.5116	1.0000	1.0000
		25	0.9989	0.6821	1.0000	1.0000
		75	0.9883	0.7514	1.0000	1.0000
.995	0.5	10	0.9813	0.7328	1.0000	1.0000
		25	0.9719	0.9096	1.0000	1.0000
		75	0.9933	0.9130	1.0000	1.0000
	1.0	10	0.9709	0.9015	1.0000	1.0000
		25	0.9991	0.8996	1.0000	1.0000
		75	0.9949	0.9267	1.0000	1.0000
	20.0	10	0.9723	0.6432	1.0000	1.0000
		25	0.9923	0.7539	1.0000	1.0000
		75	0.9971	0.9489	1.0000	1.0000

## V. CONCLUSIONS AND RECOMMENDATIONS

The lower interval estimation procedure for reliability of coherent systems which was developed in Chapter II appears to be accurate, easy to use, and applicable to coherent systems. Although this procedure assumes that failure times of all components of the system are independent and have *exponential* probability distributions, it can be easily extended to systems with component failure distributions that can be transformed into *exponential* failure distributions ; e.g., *Weibull* distribution with known shape parameter. This procedure has potential for being combined with a similar procedure for systems with cyclical components. The combined procedure would provide for use of *binomial* component test data and *exponential* component test data to compute lower confidence limits on the reliability of coherent systems with both cyclic and continuous components. Such an extension could use a failure rate ratio estimation procedure similar to that developed in this thesis. Such a method should be explored.

The interval estimation method for the reliability of a system with components that have *Weibull* failure times is not sufficiently accurate to be applied to systems that have 10 or fewer components each with ten or fewer tests. This procedure needs further study and refinement.

The approximate lower confidence limit for component reliability  $P(X > y)$  when  $X$  is *normally* distributed with unknown mean and variance is very accurate. It does not require an extensive set of tables such as those developed by Owen and Hua[Ref. 11], but only requires the use of the standard  $t$  tables.

## APPENDIX A. MLE OF WEIBULL PARAMETERS BY THE NEWTON - RAPHSON METHOD

Let  $X \sim WEI(\alpha, \beta)$ . Then the likelihood function for the first  $r$  ordered observations from a random sample of size  $n$  is given by

$$\begin{aligned} f(x_{1:n}, \dots, x_{r:n}) &= \frac{n!}{(n-r)!} \left[ \prod_{i=1}^r f_X(x_{i:n}) \right] [1 - F_X(x_{r:n})]^{n-r} \\ &= \frac{n!}{(n-r)!} \left( \frac{\beta}{\alpha} \right)^r \prod_{i=1}^r \left( \frac{x_{i:n}}{\alpha} \right)^{\beta-1} \exp \left\{ - \left[ \sum_{i=1}^r \left( \frac{x_{i:n}}{\alpha} \right)^\beta + (n-r) \left( \frac{x_{r:n}}{\alpha} \right)^\beta \right] \right\} \end{aligned}$$

Setting the partial derivatives of this likelihood with respect to  $\alpha$  and  $\beta$  equal to zero gives the MLE's  $\hat{\alpha}$  and  $\hat{\beta}$  as solutions to the equations

$$\frac{\sum_{i=1}^n x_i^{\hat{\beta}} \ln x_i}{\sum_{i=1}^n x_i^{\hat{\beta}}} - \frac{1}{\hat{\beta}} = \frac{1}{n} \sum_{i=1}^n \ln x_i$$

and

$$\hat{\alpha} = \left[ \frac{\sum_{i=1}^n x_i^{\hat{\beta}}}{n} \right]^{\frac{1}{\hat{\beta}}}$$

where  $n = r$ . It can be shown that these equations have unique solutions which are the maximum likelihood estimates. The NEWTON - RAPHSON method for solving an equation  $g(\hat{\beta}) = 0$  is to determine successive approximations  $\hat{\beta}_j$ , where  $\hat{\beta}_{j+1} = \hat{\beta}_j - g(\hat{\beta}_j)/g'(\hat{\beta}_j)$ . Therefore, the estimates of  $\alpha$  and  $\beta$  can be solved by letting

$$g(\hat{\beta}) = \frac{\sum_{l=1}^n x_l^{\hat{\beta}} \ln x_l}{\sum_{l=1}^n x_l^{\hat{\beta}}} - \frac{1}{\beta} - \frac{1}{n} \sum_{l=1}^n \ln x_l .$$

The derivative of  $g(\hat{\beta})$  is

$$g'(\hat{\beta}) = \frac{\sum_{l=1}^n x_l^{\hat{\beta}} (\ln x_l)^2}{\sum_{l=1}^n x_l^{\hat{\beta}}} - \frac{\sum_{l=1}^n x_l^{\hat{\beta}} \ln x_l}{\sum_{l=1}^n x_l^{\hat{\beta}}} + \left( \frac{1}{\hat{\beta}} \right)^2 .$$





C  
C  
C  
C

\*  
\*\*\*\*\*

PARAMETER (NN = 500)

REAL TIME(15), ALPHA(2), ZALPHA(2), RSYS(2), LAMBDA(15), P  
REAL LAMMAX, LAMHAT(15), B(100), RSTAR(15), LAMHM  
REAL RATIO1(15), RATIO2(15), BIGLAM, DIFF(15)  
REAL LOMIT(15,100), CTIME(15,100), ROMIT(15,100), T(15)  
REAL ROMSUM, SUM1, SUM2, LAMHST, R1(NN), R2(NN), KEY1(NN)  
REAL RVAL1(15), RVAL2(15), CLR1(15), CLR2(15), KEY2(NN)  
REAL DIFFR1(15), DIFFR2(15), R(15)

INTEGER SAMPLE(15), N(2), DF, CASE

DATA N / 5,0 /  
DATA RSYS / .9, .975 /  
DATA TIME / 2,3,7,8,10,3,7,10,1,7,8,3,10,1,8 /  
DATA SAMPLE / 30,63,75,98,26,15,7,5,30,20,10,7,13,21,30 /  
DATA ALPHA / .2, .05 /  
DATA ISEED / 1736 /

C /\* SUBROUTINE ZTABLE COMPUTES THE RIGHT PERCENT POINT ZALPHA \*/  
C /\* FROM RIGHT CUMULATIVE PROBABILITY ALPHA \*/

DO 10 I = 1, 2  
CALL ZTABLE(ALPHA(I), ZALPHA(I))  
10 CONTINUE

CASE = 0

/\* II IS INDEX FOR N \*/

DO 150 II = 1, 2

C /\* COMPUTE THE DEGREE OF FREEDOM FOR CHI-SQUARE \*/

DF = 0.  
DO 20 I = 1, N(II)  
DF = DF + SAMPLE(I)  
20 CONTINUE  
DF = 2 \* DF

C /\* FINDING COMPONENT TYPE THAT HAS THE MINIMUM NUMBER \*/  
C /\* OF SAMPLE SIZE \*/

NSTAR = 999  
DO 25 I = 1, N(II)  
IF (SAMPLE(I) .LE. NSTAR) THEN  
NSTAR = SAMPLE(I)  
ENDIF  
25 CONTINUE

```

/* JJ IS INDEX FOR RSYS                                */
DO 140 JJ = 1, 2

C      /* COMPUTE LAMBDA FROM THE GIVEN EQUATION AND    */
C      /* FIND THE BIGGEST LAMBDA                        */

BIGLAM = 0
DO 30 K = 1, N(II)
    LAMBDA(K) = ( -ALOG(RSYS(JJ)) / N(II)) / TIME(K)
    IF( LAMBDA(K) .GE. BIGLAM) BIGLAM = LAMBDA(K)
    R(K) = EXP( - LAMBDA(K) * TIME(K) )
30    CONTINUE

C      /* COMPUTE CHI-SQUARE VALUE FOR GIVEN ALPHA AND DF */

/* LL IS INDEX FOR ALPHA                                */
DO 130 LL = 1, 2

    IF ( DF .EQ. 1 ) THEN
        P = ALPHA(LL) / 2
        CALL ZTABLE(P, ZALPHA(LL))
        CHISQR = ZALPHA(LL) ** 2

    ELSE IF ( DF .EQ. 2 ) THEN
        CHISQR = -2 * ALOG(ALPHA(LL))

    ELSE IF ( DF .GE. 3 ) THEN
        CHISQR = DF * (1 - 2. / (9 * DF) +
            ZALPHA(LL) * SQRT( 2. / (9 * DF))) ** 3
    *
    ENDIF

CASE = CASE + 1
DIFF(CASE) = 0

DO 120 L = 1, NN

    LAMMAX = -99.
    DO 50 I = 1, N(II)

C      /* GENERATE EXPONENTIAL RANDOM                    */
C      /* NUMBERS WITH MU = 1                            */

        CALL LEXPN(ISEED, B, SAMPLE(I), 1, 0)
        T(I) = 0

        DO 40 J = 1, SAMPLE(I)

C      /* CONVERT TO EXPONENTIAL RANDOM                  */
C      /* NUMBERS WITH MU = LAMBDA AND                   */

```

```

C          /* ADD THOSE FOR EACH COMPONENT */
C          /* TYPE */

          B(J) = B(J) / LAMBDA(I)
          T(I) = T(I) + B(J)
          CTIME(I,J) = B(J)

40        CONTINUE

          LAMHAT(I) = SAMPLE(I) / T(I)

C          /* FINDING MAXIMUM LAMBDA HAT AND ITS */
C          /* INDEX */

          IF ( LAMHAT(I) .GE. LAMMAX ) THEN
            M = I
            LAMMAX = LAMHAT(I)
          ENDIF

50        CONTINUE

C          /* RATIO1 IS FOR WITHOUT JACKKNIFE */
C          /* RATIO2 IS FOR WITH JACKKNIFE */

          DO 60 I = 1, N(II)
            RATIO1(I) = LAMBDA(I) / BIGLAM
            RATIO2(I) = LAMHAT(I) / LAMMAX
60        CONTINUE

C          /* PART OF JACKKNIFE METHOD FOR LAMBDA */
C          /* WITH OMIT 1 VARIABLE EACH TIME */

          DO 90 I = 1, N(II)
            DO 80 J = 1, SAMPLE(I)

              LOMIT(I,J) = 0.
              DO 70 K = 1, SAMPLE(I)

                IF (J .NE. K) THEN
                  LOMIT(I,J) = LOMIT(I,J) + CTIME(I,K)
                ENDIF

70            CONTINUE

            LOMIT(I,J) = (SAMPLE(I)-1) / LOMIT(I,J)

80          CONTINUE
90        CONTINUE

```

```

C          /* ADAPT ABOVE RESULT TO OUR EQUATION TO      */
C          /* GET THE RELIABILITY AND TRUE CONFIDENCE    */
C          /* LIMIT                                       */

SUM1 = 0.
SUM2 = 0.
SUM3 = 0.
SUM4 = 0.

DO 110 I = 1, N(II)

C          /* NON JACKKNIFING ( ORIGINAL )              */

SUM1 = SUM1 + RATIO1(I) * T(I)
SUM2 = SUM2 + RATIO1(I) * TIME(I)

C          /* WITH JACKKNIFING                          */

ROMSUM = 0.
DO 100 J = 1, NSTAR
    ROMIT(I,J) = LOMIT(I,J) / LOMIT(M,J)
    ROMSUM = ROMSUM + ROMIT(I,J)
100 CONTINUE

    RSTAR(I) = NSTAR * RATIO2(I) -
    (NSTAR - 1) * ROMSUM / NSTAR
    SUM3 = SUM3 + RSTAR(I) * T(I)
    SUM4 = SUM4 + RSTAR(I) * TIME(I)
110 CONTINUE

C          /* R1 ; RELIABILITY OF A SYSTEM WITHOUT      */
C          /* JACKKNIFE                                  */
C          /* R2 ; RELIABILITY OF A SYSTEM WITH         */
C          /* JACKKNIFE                                  */

LAMHM = CHISQR / (2 * SUM1)
R1(L) = EXP( - LAMHM * SUM2 )

LAMHST = CHISQR / (2 * SUM3)
R2(L) = EXP( - LAMHST * SUM4 )

IF ( ABS(R1(L) - R2(L)) .GE. DIFF(CASE) ) THEN
    DIFF(CASE) = ABS(R1(L) - R2(L))
    DIFFR1(CASE) = R1(L)
    DIFFR2(CASE) = R2(L)
ENDIF

120 CONTINUE

C          /* NONIMSL LIBRARY 'SHSORT' WILL SORT R1, R2 */
C          /* BY SHELL SORT ALGORITHM                   */

```

```

        CALL SHSORT(R1, KEY1, NN)
        CALL SHSORT(R2, KEY2, NN)

        MM = NN * (1 - ALPHA(LL))

        RVAL1(CASE) = R1(MM)
        RVAL2(CASE) = R2(MM)

C          /* SUBROUTINE FINDJ FINDS THE INDEX OF R1, R2      */
C          /* WHICH THE VALUE OF IT IS CLOSEST TO RSYS.      */

        CALL FINDJ(R1, NN, RSYS(JJ), J1)
        CALL FINDJ(R2, NN, RSYS(JJ), J2)

        CLR1(CASE) = J1 / FLOAT(NN)
        CLR2(CASE) = J2 / FLOAT(NN)

130          CONTINUE
140          CONTINUE
150 CONTINUE

        WRITE(6,600)
        WRITE(6,650)
        WRITE(6,670)

        CASE = 1
        DO 210 II = 1, 2
            DO 200 JJ = 1, 2
                DO 190 LL = 1, 2

                    WRITE(6,700) N(II), RSYS(JJ), ALPHA(LL), RVAL1(CASE),
*                     RVAL2(CASE), DIFF(CASE), CLR1(CASE), CLR2(CASE)

                    WRITE(6,888) DIFFR1(CASE), DIFFR2(CASE)
                    CASE = CASE + 1

190          CONTINUE
200          CONTINUE
                WRITE(6,777) ( SAMPLE(J), J=1,N(II) )
                WRITE(6,999) ( R(J), J=1,II )
210 CONTINUE

600 FORMAT('1',5(/),7X,'**** RELIABILITY OF SERIES SYSTEM ****')
650 FORMAT(///,T50,'R1, CL1 ; WITHOUT JACKKNIFING',
*         /,T50,'R2, CL2 ; WITH JACKKNIFING')
670 FORMAT(///,T6,'NUMBER OF',T19,'RELIABILITY',T33,'ALPHA',T46,'R1',
*         T56,'R2',T63,'MAX (R1 - R2)',T79,'TRUE',T87,'TRUE',/,
*         T6,'COMPONENTS',T19,'OF SYSTEM',T79,'C.L. 1',T87,'C.L. 2',
*         /,T5,89('-'))

```

```

700 FORMAT(/,T8,I5,T22,F5.3,T33,F5.2,T43,F7.4,T53,F7.4,T65,F8.4,T78,
*       F7.4,T86,F7.4)

777 FORMAT(/,T3,'SAMPLE SIZE ARE ',5(2X,I3) )
888 FORMAT(T60,'R1=',F6.4,' R2=',F6.4)
999 FORMAT(/,T3,'R(I) ; ',5(1X,F5.3))

```

```

STOP
END

```

```

*****
*
*****

```

```

SUBROUTINE ZTABLE(ALPHA,ZALPHA)
C
C  << SUBROUTINE ZTABL2 COMPUTES RIGHT PERCENT POINT ZALPHA FROM  >>
C  << RIGHT CUMULATIVE PROBABILITY ALPHA                        >>
C
REAL ALPHA, ZALPHA

IF ((ALPHA .GT. 0.0) .OR. (ALPHA .LT. 1)) THEN

    W = - ALOG(4 * ALPHA * ( 1 - ALPHA ))
    ZALPHA = SQRT(W * (2.06118 - ( 5.72622 / (W + 11.6406))))

    IF (ALPHA .GT. 0.5) THEN
        ZALPHA = - ZALPHA
    ENDIF
ENDIF

RETURN
END

```

```

*****
*
*****

```

```

SUBROUTINE SHSORT(A,KEY,N)
DIMENSION A(N),KEY(N)
M1=1
6 M1=M1*2
  IF (M1 .LE. N) GO TO 6
  M1=M1/2-1
  MM=MAX0(M1/2,1)
  GO TO 21
20 MM=MM/2
  IF (MM .LE. 0) GO TO 100
21 K=N-MM

```

```

22 DO 1 J=1,K
    II=J
11 IM=II+MM
    IF (A(IM) .GE. A(II)) GO TO 1
    TEMP=A(II)
    IT=KEY(II)
    A(II)=A(IM)
    KEY(II)=KEY(IM)
    A(IM)=TEMP
    KEY(IM)=IT
    II=II-MM
    IF (II .GT. 0) GO TO 11
1 CONTINUE
GO TO 20
100 RETURN
END

```

```

*****
*
*****

```

```

SUBROUTINE FINDJ(A, NN, R, J)
C
C << SUBROUTINE FINDJ FINDS THE INDEX OF ARRAY A WHICH THE >>
C << VALUE OF IT IS CLOSEST TO R. >>
C
REAL A(NN), R, VALUE
INTEGER J

VALUE = ABS(A(NN) - R)

DO 100 I = NN-1, 1, -1

    IF (ABS(A(I) - R) .LT. VALUE) THEN
        VALUE = ABS(A(I) - R)
    ELSE
        J = I + 1
        RETURN
    ENDIF

100 CONTINUE

RETURN
END

```



## APPENDIX C. FORTRAN CODE FOR INTERVAL ESTIMATION PROCEDURE - WEIBULL CASE

PROGRAM WEIBUL

```

C
C *****
C
C *
C * THIS PROGRAM COMPUTES THE RELIABILITY OF A SERIES SYSTEM
C * USING TWO DIFFERENT METHODS FOR THE CASE WHEN FAILURE
C * OF EACH COMPONENTS IS WEIBULLY DISTRIBUTED.
C * AND ALSO COMPARES THE ESTIMATE OF SHAPE PARAMETERS ( BETA )
C * WHICH IS COMPUTED FROM TWO DIFFERENT METHODS.
C *
C * THE SERIES SYSTEM CONSIDERED IN THIS PROGRAM HAS
C * N COMPONENT TYPES AND EACH COMPONENT HAS SAME NUMBER OF
C * SAMPLE SIZES.
C *
C * BELOWS ARE GIVEN OR ASSUMED ;
C *
C *      BETA ; SHAPE PARAMETER OF WEIBULL DISTRIBUTION
C *      ALPHA ; SIGNIFICANCE LEVEL
C *      X ; TEST TIME
C *      RSYS ; RELIABILITY OF A SERIES SYSTEM
C *
C * THESE ARE VARIABLES USED ;
C *
C *      BETHAT ; BETA HAT FROM THE FORMULA
C *      BETNEW ; BETA HAT FROM NEWTON - RAPHSON METHOD
C *      CHISQR ; CHI-SQUARE VALUE FOR GIVEN ALPHA AND DF
C *      CLR ; TRUE CONFIDENCE LIMIT FROM THE FORMULA
C *      CLRNEW ; TRUE CONFIDENCE LIMIT FROM THE N-R METHOD
C *      EXPO ; EXPONENTIAL RANDOM NUMBERS WITH MU=1
C *      KSUBM ; K SUB M VALUE
C *      LAMBDA ; SCALE PARAMETER OF WEIBULL DISTRIBUTION
C *      LAMBIG ; MAXIMUM VALUE OF LAMBDA FROM THE N-R METHOD
C *      LAMHAT ; ESTIMATES OF LAMBDA FROM THE FORMULA
C *      LAMMAX ; MAXIMUM VALUE OF LAMBDA FROM THE FORMULA
C *      LAMMU ; FINALLY COMPUTED LAMBDA FROM THE FORMULA
C *      LAMSTR ; LAMBDA TO THE BETA
C *      LAMNEW ; ESTIMATES OF LAMBDA FROM THE N-R METHOD
C *      LAMUNR ; FINALLY COMPUTED LAMBDA FROM THE N-R METHOD
C *      RATIO ; RATIO OF LAMBDA FOR THE FORMULA
C *      RATNEW ; RATIO OF LAMBDA FOR THE N-R METHOD
C *      RHAT ;  $R( 500 * (1-ALPHA) )$  FOR THE FORMULA
C *      RHTNEW ;  $R( 500 * (1-ALPHA) )$  FOR THE N-R METHOD
C *      XBENew ; X TO THE BETNEW
C *      XHAT ; SUM OF XIJHAT
C *      XIJHAT ; W TO THE BETHAT
C *      XIJNEW ; W TO THE BETNEW
C *      XNEW ; SUM OF XIJNEW
C *      XTOBET ; X TO THE BETHAT
C *      W,WEIB ; WEIBULL RANDOM NUMBERS

```

```

C      *      ZALPHA ; RIGHT PERCENTILE POINT (NORMAL DISTRIBUTION)      *
C      *
C      ****
C
C      PARAMETER ( N=5, M=30 , NN= 500 )
C      PARAMETER ( N=15, M=30 , NN= 500)

REAL      BETA(N), LAMBDA(N), X(N), XHAT(N), XTOBET(N), XX(N,M)
REAL      W(N,M), Y(N,M), BETHAT(N), WBHAT(N,M), LAMHAT(N)
REAL      RATIO(N), LAMSTR(N), LAMMAX, RSYS(2), KSUBM(N), LAMMU
REAL      EXPO(M), ALPHA(2), ZALPHA(2), RHAT(10), RSL(NN), CHISQR
REAL      B(M), KEY(M), KEY1(NN), KEY2(NN), XIJHAT(N,M)
REAL      WEIB(M), BETNEW(N), XBENNEW(N), XNEW(N), XIJNEW(N,M)
REAL      LAMNEW(N), LAMBIG, RATNEW(N), LAMUNR, RSLNEW(NN)
REAL      RHTNEW(10), CLR(10), CLRNEW(10)
REAL      BHTBAR, BNRBAR, BHTMSE, BNRMSE

INTEGER   S(N), DF, ICOUNT, SAMPLE(N), CASE

DATA ISEED / 1736 /
DATA ALPHA / .2, .05 /
DATA RSYS / .90, .975 /

C      DATA BETA / 1.2,1.4,1.6,1.8,1.5 /
C      DATA BETA /1.2,1.4,1.6,1.8,1.5,1.3,1.7,1.5,1.2,1.6,1.9,1.8,1.4,
C      *      1.6,1.1/
C      DATA BETA / 2.2,2.4,2.6,2.8,2.5 /
C      DATA BETA /2.2,2.4,2.6,2.8,2.5,2.3,2.7,2.5,2.2,2.6,2.9,2.8,2.4,
C      *      2.6,2.1/

C      DATA X / 2,3,7,8,10/
C      DATA X /2,3,7,8,10,3,7,10,1,7,8,3,10,1,8/

C      DATA SAMPLE /9,7,10,8,6/
C      DATA SAMPLE /30,21,10,15,26/
C      DATA SAMPLE / 30,63,75,98,26 /

C      DATA SAMPLE /6,7,5,6,7,8,9,5,8,7,9,10,7,9,6/
C      DATA SAMPLE /3,7,10,15,20,15,7,5,30,20,10,7,13,21,30/
C      DATA SAMPLE /15,40,35,17,26,67,50,65,80,32,95,100,15,45,30/

DATA SAMPLE / 15 * 15 /

CASE = 1

DO 10 I = 1, N
      IF ( SAMPLE(I) .LE. 15) KSUBM(I) = 1.40
      IF ( SAMPLE(I) .LE. 30) KSUBM(I) = 1.50
10 CONTINUE

DO 220 JJ = 1, 2

C      /* FINDING THE LAMBDA AND LAMBDA STAR FROM THE GIVEN DATA */
C      DO 20 I = 1, N

```

```

        LAMBDA(I) = (( - ALOG(RSYS(JJ)) / N) ** (1./BETA(I)))/ X(I)
        LAMSTR(I) = LAMBDA(I) ** BETA(I)
        S(I)      = 0.84 * SAMPLE(I) - 0.5
20    CONTINUE

C      /* SUBROUTINE ZTABLE COMPUTES THE RIGHT PERCENT POINT ZALPHA */
C      /* FROM RIGHT CUMULATIVE PROBABILITY ALPHA */

        DO 40 I = 1, 2
            CALL ZTABLE(ALPHA(I), ZALPHA(I))
40    CONTINUE

C      /* COMPUTE THE DEGREE OF FREEDOM FOR CHI-SQUARE */

        DF = 0
        DO 60 I = 1, N
            DF = DF + SAMPLE(I)
60    CONTINUE
        DF = 2 * DF

C      /* COMPUTE CHI-SQUARE VALUE FOR GIVEN ALPHA AND DF */

        DO 200 LL = 1, 2

            IF ( DF .EQ. 1 ) THEN
                P = ALPHA(LL) / 2
                CALL ZTABLE(P, ZALPHA(LL))
                CHISQR = ZALPHA(LL) ** 2

            ELSE IF ( DF .EQ. 2 ) THEN
                CHISQR = -2 * ALOG(ALPHA(LL))

            ELSE IF ( DF .GE. 3 ) THEN
                CHISQR = DF * (1 - 2./(9 * DF) +
*                ZALPHA(LL) * SQRT( 2./(9 * DF))) ** 3
            ENDIF

            LAMMAX = 0
            LAMBIG = 0

            DO 180 ITER = 1, NN

                DO 140 I = 1, N

                    /* GENERATE EXPONENTIAL RANDOM NUMBER WITH MU=1 */
                    CALL LEXPN(ISEED, EXPO, SAMPLE(I), 1, 0)

                    /* CONVERT EXPONENTIAL RANDOM NUMBER WITH MU=1 */
                    /* TO MU=LAMBDA AND GET WEIBULL RANDOM NUMBERS */
                    DO 80 J = 1, SAMPLE(I)
                        XX(I,J) = EXPO(J) / LAMSTR(I)
                        W(I,J) = XX(I,J) ** (1/BETA(I))
                        Y(I,J) = ALOG(W(I,J))
                        WEIB(J) = W(I,J)

```

```

      B(J)      = Y(I,J)
80      CONTINUE

      /* SUBROUTINE SHSORT WILL SORT ARRAY B IN      */
      /* ASCENDING ORDER BY SHELL SORT ALGORITHM      */
      CALL SHSORT(B, KEY, SAMPLE(I))                */

      /* FINDING BETA HAT (BETHAT) BY THE FORMULA      */
      /*                                               */

      SUM1 = 0
      SUM2 = 0

      DO 100 J = 1, S(I)
          SUM1 = SUM1 + B(J)
100      CONTINUE

      DO 120 J = S(I)+1, SAMPLE(I)
          SUM2 = SUM2 + B(J)
120      CONTINUE

      *      BETHAT(I) = (SAMPLE(I)) * KSUBM(I) /
      (S(I)*SUM2 / (SAMPLE(I) - S(I)) - SUM1)

      TEMP = BETA(I)

      /* SUBROUTINE NEWTON WILL COMPUTE THE ESTIMATE  */
      /* OF BETA (BETNEW) BY NEWTON-RAPHSON METHOD    */
      CALL NEWTON(WEIB, SAMPLE(I), TEMP, BETNEW(I))  */

      XTOBET(I) = X(I) ** BETHAT(I)
      XBENNEW(I) = X(I) ** BETNEW(I)

      XHAT(I) = 0.
      XNEW(I) = 0.

      DO 130 J = 1, SAMPLE(I)
          XIJHAT(I,J) = W(I,J) ** BETHAT(I)
          XHAT(I)      = XHAT(I) + XIJHAT(I,J)

          XIJNEW(I,J) = W(I,J) ** BETNEW(I)
          XNEW(I)      = XNEW(I) + XIJNEW(I,J)
130      CONTINUE

      LAMHAT(I) = SAMPLE(I) / XHAT(I)
      LAMNEW(I) = SAMPLE(I) / XNEW(I)

      IF (LAMHAT(I) .GT. LAMMAX ) THEN
          LAMMAX = LAMHAT(I)
      ENDIF

      IF (LAMNEW(I) .GT. LAMBIG ) THEN
          LAMBIG = LAMNEW(I)
      ENDIF
140      CONTINUE

      SUM3 = 0

```

```

SUM3N = 0
SUM4 = 0
SUM4N = 0

DO 160 I = 1, N
    RATIO(I) = LAMHAT(I) / LAMMAX
    RATNEW(I) = LAMNEW(I) / LAMBIG
    SUM3 = SUM3 + RATIO(I) * XHAT(I)
    SUM4 = SUM4 + RATIO(I) * XTOBET(I)

    SUM3N = SUM3N + RATNEW(I) * XNEW(I)
    SUM4N = SUM4N + RATNEW(I) * XBENNEW(I)

160    CONTINUE

    LAMMU = CHISQR / ( 2 * SUM3 )
    RSL(ITER) = EXP( - LAMMU * SUM4 )

    LAMUNR = CHISQR / ( 2 * SUM3N )
    RSLNEW(ITER) = EXP( - LAMUNR * SUM4N )

180    CONTINUE

    CALL SHSORT(RSL, KEY1, NN)
    CALL SHSORT(RSLNEW, KEY2, NN)

    KK = ( 1 - ALPHA(LL)) * NN

    /* RHAT IS THE RELIABILITY OF THE SERIES SYSTEM COMPUTED */
    /* BY THE FORMULA */
    /* RHTNEW IS THE RELIABILITY OF THE SERIES SYSTEM COMPUTED */
    /* BY THE NEWTON - RAPHSON METHOD */

    RHAT(CASE) = RSL(KK)
    RHTNEW(CASE) = RSLNEW(KK)

    /* SUBROUTINE FINDJ WILL FIND THE TRUE CONFIDENCE LIMIT */
    CALL FINDJ(RSL, NN, RSYS(JJ), J1)
    CALL FINDJ(RSLNEW, NN, RSYS(JJ), J2)

    CLR(CASE) = J1 / FLOAT(NN)
    CLRNEW(CASE) = J2 / FLOAT(NN)

    CASE = CASE + 1

200    CONTINUE

220    CONTINUE

    DO 240 I = 1, N
        WRITE(6,500) BETA(I), SAMPLE(I)
240    CONTINUE

    WRITE(6,550) N, NN
    WRITE(6,600)

```

```
WRITE(6,650)
WRITE(6,670)
```

```
CASE = 1
DO 280 JJ = 1, 2
  DO 260 LL = 1, 2
```

```
      WRITE(6,700) N,RSYS(JJ),ALPHA(LL),RHAT(CASE),RHTNEW(CASE),
*          CLR(CASE), CLRNEW(CASE)
      CASE = CASE + 1
```

```
260      CONTINUE
280 CONTINUE
```

```
500 FORMAT(T10,'INITIAL BETA          : ',3X,F4.1,
*          T45,'NUMBER OF SAMPLE SIZES : ',2X,I3)
550 FORMAT(T10,'NUMBER OF COMPONENTS  : ',2X,I3,
*          /,T10,'NUMBER OF REPLICATIONS : ',2X,I3)
600 FORMAT('1',5(/),7X,'***** RELIABILITY OF SERIES SYSTEM *****')
650 FORMAT(///,T35,'R1, CL1 ; USING THE FORMULAR',
*          /,T35,'R2, CL2 ; USING THE NEWTON RAHPSON METHOD')
670 FORMAT(///,T6,'NUMBER OF',T19,'RELIABILITY',T33,'ALPHA',T46,'R1',
*          T56,'R2',T66,'TRUE',T74,'TRUE',/,
*          T6,'COMPONENTS',T19,'OF SYSTEM',T66,'C.L. 1',T74,'C.L. 2',
*          /,T5,76(' '))
700 FORMAT(/,T8,I5,T22,F5.3,T33,F5.2,T43,F7.4,T53,F7.4,T65,
*          F7.4,T73,F7.4)
```

```
STOP
END
```

```
*****
*
*****
```

```
SUBROUTINE ZTABLE(ALPHA,ZALPHA)
```

```
C
C  << SUBROUTINE ZTABL2 COMPUTES RIGHT PERCENT POINT ZALPHA FROM  >>
C  << RIGHT CUMULATIVE PROBABILITY ALPHA                        >>
C
```

```
REAL ALPHA, ZALPHA
```

```
IF ((ALPHA .GT. 0.0) .OR. (ALPHA .LT. 1)) THEN
```

```
  W = - ALOG(4 * ALPHA * ( 1 - ALPHA ))
  ZALPHA = SQRT(W * (2.06118 - ( 5.72622 / (W + 11.6406))))
```

```
  IF (ALPHA .GT. 0.5) THEN
    ZALPHA = - ZALPHA
  ENDIF
```

ENDIF

RETURN  
END

\*\*\*\*\*  
\*  
\*\*\*\*\*

```
      SUBROUTINE SHSORT(A,KEY,N)
      DIMENSION A(N),KEY(N)
      M1=1
6     M1=M1*2
      IF (M1 .LE. N) GO TO 6
      M1=M1/2-1
      MM=MAX0(M1/2,1)
      GO TO 21
20    MM=MM/2
      IF (MM .LE. 0) GO TO 100
21    K=N-MM
22    DO 1 J=1,K
        II=J
11    IM=II+MM
        IF (A(IM) .GE. A(II)) GO TO 1
        TEMP=A(II)
        IT=KEY(II)
        A(II)=A(IM)
        KEY(II)=KEY(IM)
        A(IM)=TEMP
        KEY(IM)=IT
        II=II-MM
        IF (II .GT. 0) GO TO 11
1     CONTINUE
      GO TO 20
100   RETURN
      END
```

\*\*\*\*\*  
\*  
\*\*\*\*\*

```
      SUBROUTINE NEWTON(TIME, M, BETA, BETNEW )
C
C     << SUBROUTINE NEWTON WILL COMPUTE THE ESTIMATE OF BETA (BETHAT) >>
C     << BY NEWTON - RAPHSON METHOD >>
C
      REAL      TIME(M), LNTIME(100), A(3), LNTS
      INTEGER   R
C
      DATA TS / 6 /
C
      C      = 0
      ITER = 0
```

```

      R      = M
C      LNTS = ALOG(TS)

      DO 20 I = 1, R
          LNTIME(I) = ALOG(TIME(I))
          C = C + LNTIME(I)
20     CONTINUE

      C = C / R

30     DO 60 J = 1, 3
          SUM = 0

          DO 40 K = 1, R

              IF ( J .EQ. 1 ) THEN
                  SUM = SUM + TIME(K) ** BETA
              ELSE
                  SUM = SUM + ((TIME(K) ** BETA)*(LNTIME(K) ** (J-1)))
              ENDIF
40         CONTINUE

          A(J) = SUM

60     CONTINUE

      /* FUNCTION FPRIME IS THE DERIVATIVES OF FUNCTION F          */
      QUOT = A(2) / A(1)
      FPRIME = A(3) / A(1) - (QUOT**2) + ((1/BETA)**2)
      F = QUOT - (1 / BETA) - C

      /* BETA IS UPDATED EACH TIME AND CHECK IF IT CONVERGES      */
      BETA = BETA - F / FPRIME

      ITER = ITER + 1
      IF (BETA .GT. 25.) GOTO 100

      IF ( ABS(F) .GT. 0.0001 ) GOTO 30

      ALPHA = (A(1) / R) ** (1/BETA)
      BETNEW = BETA

      RETURN

100    WRITE(6,*) 'DID NOT CONVERGE'
        WRITE(6,*) 'TRY AGAIN WITH BETTER ESTIMATE OF BETA'

      RETURN
      END

```

```

*****
*
*****

```



```

SUBROUTINE FINDJ(A, NN, R, J)
C
C  << SUBROUTINE FINDJ FINDS THE INDEX OF ARRAY A  WHICH THE  >>
C  << VALUE OF IT IS CLOSEST TO R.  >>
C
REAL A(NN), R, VALUE
INTEGER J

VALUE = ABS(A(NN) - R)

DO 100 I = NN-1, 1, -1

  IF (ABS(A(I) - R) .LT. VALUE) THEN
    VALUE = ABS(A(I) - R)
  ELSE
    J = I + 1
    RETURN
  ENDIF

100 CONTINUE

RETURN
END

```

# APPENDIX D. FORTRAN CODE FOR INTERVAL ESTIMATION PROCEDURE - NORMAL CASE

```

PROGRAM NORMAL
C
C *****
C *
C * THIS PROGRAM DETERMINE THE ACCURACY OF AN APPROXIMATE
C * LOWER CONFIDENCE BOUND FOR P( X > Y ).
C *
C * PROGRAM NORMAL IS THE CASE WHEN Y IS GIVEN A VALUE Y0
C * & X IS NORMALLY DISTRIBUTED WITH
C * UNKNOWN PARAMETERS.
C *
C *****
C
REAL Y0, P, ZP, MUX, SUMX, SUMX2, XBAR
REAL TEMP1, TEMP2, TEMP3, SIGHAT
REAL R(3), SIGMAX(3), ALPHA(2), X(100), Y(100)
REAL RL1(54,1000), ARL1(1000), BRL1(54), KEY(1000), CIRL1(54)
REAL T1RL1(54), T1CI1(54), T2RL1(54), T2CI1(54)
REAL TRL1(2), TCI1(2)
REAL ZHAT(1000), ZKNIFE(54), ZVAR(54), ZBAR(54)
REAL MUJUNK(54)

INTEGER NUMX(3), NUMY(3), CASE, LINE

DATA R /.95,.99,.995/, SIGMAX /.5,1,20/, NUMX /10,25,75/
DATA NUMY /10,25,75/, ALPHA / .2, .1/
DATA ISEED, JSEED / 4875,7981 /
DATA Y0 / 400 /

CASE = 0

C /* II IS THE INDEX FOR R. R(1) = .95, R(2) = .99, R(3) = .995 */
DO 500 II = 1, 3

C /* P IS THE RIGTH(UPPER) CUMULATIVE PROBABILITY */
P = 1 - R(II)

C /* SUBROUTINE ZTABL2 COMPUTES RIGHT PERCENT POINT ZP */
C /* FROM RIGHT CUMULATIVE PROBABILITY P */
CALL ZTABL2( P, ZP )

C /* JJ IS THE INDEX FOR SIGMA OF X. */
C /* SIGMAX(1) = .5, SIGMAX(2) = 1, SIGMAX(3) = 3 */

```

```

DO 400 JJ = 1, 3

    MUX = ZP * SIGMAX(JJ) + Y0

C      /* KK IS THE INDEX OF NUMBER OF X.                */
C      /* NUMX(1) = 10, NUMX(2) = 25, NUMX(3) = 75        */
C      DO 300 KK = 1, 3                                     */

C      /* LL IS THE INDEX FOR ALPHA.                      */
C      /* ALPHA(1) = .2, ALPHA(2) = .1                   */
C      DO 200 LL = 1, 2                                     */

        CALL ZTABL2(ALPHA(LL), ZALPHA)

        CASE = CASE + 1
        TEMP = (NUMX(KK) - 1.) / NUMX(KK)
        TEMPO = SQRT(TEMP)
        MUJUNK(CASE) = MUX

C      /* REPLICATE 1000 TIMES FOR EACH CASES            */
C      DO 100 I = 1, 1000                                   */

C      /* USE NORMAL RANDOM NUMBER GENERATOR TO GET      */
C      /* NUMX(KK) NUMBER OF X.                          */
C      CALL LNORM(ISEED,X,NUMX(KK),2,0)

C      /* THIS PART IS TO GET SAMPLE MEAN(XBAR) AND      */
C      /* SAMPLE VARIANCE(XVAR)                          */
C      DO 50 MM = 1, NUMX(KK)
        X(MM) = SIGMAX(JJ) * X(MM) + MUX
50      CONTINUE

C      /* SUBROUTINE VAR WILL COMPUTE SAMPLE MEAN AND    */
C      /* SAMPLE VARIANCE                                */
C      CALL VAR(X, NUMX(KK), XBAR, XVAR)

C      /* NOW WE COMPUTE THE LOWER CONFIDENCE BOUND      */
C      TEMP1 = (XBAR - Y0) / SQRT(XVAR * TEMPO)
C      TEMP2 = 1. / NUMX(KK) +
*      ((XBAR - Y0) ** 2) / (2*(NUMX(KK)+1)* XVAR)
C      TEMP1 = TEMP1 - ZALPHA * SQRT(TEMP2) * TEMP

C      /* SUBROUTINE ZTABL1 COMPUTE RIGHT CUMULATIVE PROBA- */
C      /* BILITY FROM RIGHT PERCENT POINT.                */
C      CALL ZTABL1(TEMP1, ARL1(I))

```

```

        ARL1(I) = 1. - ARL1(I)

        CALL JKNIFE(X, NUMX(KK), YO, ZHAT(I))

100      CONTINUE

        CALL VAR(ZHAT, 1000, ZBAR(CASE), ZVAR(CASE))

        SIGHAT = 1./NUMX(KK) + ZBAR(CASE)**2 / (2*(NUMX(KK)+1))
        SIGHAT = SQRT(SIGHAT) * TEMP
        SIGHAT = ZBAR(CASE) / TEMPO - SIGHAT * ZALPHA

        CALL ZTABL1(SIGHAT, ZKNIFE(CASE))

        ZKNIFE(CASE) = 1 - ZKNIFE(CASE)

C        /* NON-IMSL LIBRARY 'SHSORT' WILL SORT ARL1 BY SHELL    */
C        /* SORT ALGORITHM.                                     */

        CALL SHSORT(ARL1, KEY, 1000)

        DO 150 I = 1, 1000
            RL1(CASE,I) = ARL1(I)
150      CONTINUE

C        /* SUBROUTINE FINDJ FINDS THE INDEX OF ARL20 WHICH THE */
C        /* VALUE OF IT IS CLOSEST TO R.                       */

        CALL FINDJ(ARL1, R(II), J)

C        /* DIVIDING THE INDEX BY 1000 WILL GIVE US TRUE       */
C        /* CONFIDENCE LEVEL.                                   */

        CIRL1(CASE) = J / 1000.

        MM = 1000 * (1 - ALPHA(LL))
        BRL1(CASE) = RL1(CASE,MM)

        CALL TNYVAL(R(II), SIGMAX(JJ), NUMX(KK),
*           ALPHA(LL), ZALPHA, MUX, YO, TRL1, TCI1)

        T1RL1(CASE) = TRL1(1)
        T1CI1(CASE) = TCI1(1)
        T2RL1(CASE) = TRL1(2)
        T2CI1(CASE) = TCI1(2)

200      CONTINUE
300      CONTINUE
400      CONTINUE
500      CONTINUE

```

```

WRITE(6,600)
WRITE(6,630)
I = 1
LINE = 0
DO 550 II = 1, 3
  DO 550 JJ = 1, 3
    DO 550 KK = 1, 3

      IF (LINE .GE. 3) THEN
        WRITE(6,800)
        LINE = 0
      ENDIF

      WRITE(6,710) R(II), SIGMAX(JJ), NUMX(KK),
*               BRL1(I), BRL1(I+1), CIRL1(I), CIRL1(I+1),
*               ZKNIFE(I), ZKNIFE(I+1),
*               MUJUNK(I), MUJUNK(I+1)
      I = I + 2
      LINE = LINE + 1
550 CONTINUE

WRITE(6,610)
WRITE(6,650)
I = 1
LINE = 0
DO 560 II = 1, 3
  DO 560 JJ = 1, 3
    DO 560 KK = 1, 3

      IF (LINE .GE. 3) THEN
        WRITE(6,800)
        LINE = 0
      ENDIF

      WRITE(6,700) R(II), SIGMAX(JJ), NUMX(KK),
*               T1RL1(I), T1RL1(I+1), T1CI1(I), T1CI1(I+1)
      I = I + 2
      LINE = LINE + 1
560 CONTINUE

WRITE(6,620)
WRITE(6,650)
I = 1
LINE = 0
DO 570 II = 1, 3
  DO 570 JJ = 1, 3
    DO 570 KK = 1, 3

      IF (LINE .GE. 3) THEN
        WRITE(6,800)
        LINE = 0
      ENDIF

```

```

        WRITE(6,700) R(II), SIGMAX(JJ), NUMX(KK),
*          T2RL1(I), T2RL1(I+1), T2CI1(I), T2CI1(I+1)
        I = I + 2
        LINE = LINE + 1
570 CONTINUE

600 FORMAT('1',5(/),7X,'***** Y IS GIVEN A VALUE OF Y0 *****')
610 FORMAT('1',5(/),7X,'***** Y IS GIVEN A VALUE OF Y0 *****',
*          '//,20X,'-- X IS TRUNCATED NORMAL WITH PROBABILITY .95 --')
620 FORMAT('1',5(/),7X,'***** Y IS GIVEN A VALUE OF Y0 *****',
*          '//,20X,'-- X IS TRUNCATED NORMAL WITH PROBABILITY .90 --')

630 FORMAT(3(/),5X,' CASE ',6X,' RL1(1000*(1-ALPHA)) ',
*          4X,'TRUE CONFIDENCE LEVEL',5X,'JACKKNIFE',
*          ///,5X,'R SX N',3X,'ALPHA = .2',12X,'.1',11X,'.2',
*          12X,'.1',/,3X,13(' '),6X,25(' '),4X,21(' '),2X,16(' '),/)

650 FORMAT(3(/),5X,' CASE ',6X,' RL1(1000*(1-ALPHA)) ',
*          4X,'TRUE CONFIDENCE LEVEL',///,5X,'R SX N',3X,
*          'ALPHA = .2',12X,'.1',11X,'.2',12X,'.1',/,3X,13(' '),6X,
*          25(' '),4X,21(' '),/)

700 FORMAT(3X,F4.3,2X,F3.1,2X,I2,4(7X,F7.4))
710 FORMAT(3X,F4.3,1X,F4.1,2X,I2,4(7X,F7.4),1X,2(2X,F6.4),2(2X,F9.5))
800 FORMAT(/)

```

```

RETURN
END

```

```

*****
*
*****

```

```

SUBROUTINE ZTABL1(ZALPHA, ALPHA)
C
C << SUBROUTINE ZTABL1 COMPUTE RIGHT CUMULATIVE PROBABILITY FROM >>
C << RIGHT PERCENT POINT. >>
C
REAL PI, ALPHA, ZALPHA

PARAMETER ( PI = 3.141592 )

IF ( ZALPHA .EQ. 0.0 ) THEN
    ALPHA = 0.5
ELSE
    ALPHA = EXP( -2 * ZALPHA ** 2 / PI )
    ALPHA = SQRT(1 - ALPHA * (1 + 2*(PI-3)*ZALPHA**4/(3*PI**2)))
    ALPHA = 0.5 * ( 1 - ALPHA )

    IF ( ZALPHA .LT. 0.0 ) THEN
        ALPHA = 1 - ALPHA
    END IF

```

```

      ENDIF
ENDIF

      RETURN
      END

```

```

*****
*
*****

```

```

      SUBROUTINE ZTABL2(ALPHA,ZALPHA)
C
C      << SUBROUTINE ZTABL2 COMPUTES RIGHT PERCENT POINT ZALPHA FROM      >>
C      << RIGHT CUMULATIVE PROBABILITY ALPHA                                >>
C
      REAL ALPHA, ZALPHA

      IF ((ALPHA .GT. 0.0) .OR. (ALPHA .LT. 1)) THEN

          W = - ALOG(4 * ALPHA * ( 1 - ALPHA ))
          ZALPHA = SQRT(W * (2.06118 - ( 5.72622 / (W + 11.6406))))

          IF (ALPHA .GT. 0.5) THEN
              ZALPHA = - ZALPHA
          ENDIF
      ENDIF

      RETURN
      END

```

```

*****
*
*****

```

```

      SUBROUTINE TTABLE(ALPHA, NU, TALPHA)
C
C      << SUBROUTINE TTABLE COMPUTES RIGHT CUMULATIVE PROBABILITY      >>
C      << TALPHA FROM T-DISTRIBUTION BY GIVEN ALPHA AND NU              >>
C
      REAL ALPHA, ZALPHA, TALPHA, A1, A2, A3
      INTEGER NU

      IF ((ALPHA .GT. 0.0) .OR. (ALPHA .LT. 1)) THEN

          CALL ZTABL2(ALPHA, ZALPHA)

          A1 = (ZALPHA**2 + 1) / 4
          A2 = (5*ZALPHA**4 + 16*ZALPHA**2 + 3) / 96
          A3 = (3*ZALPHA**6 + 19*ZALPHA**4 + 17*ZALPHA**2 - 15) / 384

          TALPHA = ZALPHA * (1 + A1/NU + A2/NU**2 + A3/NU**3)

          IF ( ALPHA .GT. 0.5 ) THEN
              TALPHA = - TALPHA
          ENDIF
      ENDIF

```

ENDIF

RETURN  
END

\*\*\*\*\*  
\*  
\*\*\*\*\*

```
      SUBROUTINE SHSORT(A,KEY,N)
      DIMENSION A(N),KEY(N)
      M1=1
6     M1=M1*2
      IF (M1 .LE. N) GO TO 6
      M1=M1/2-1
      MM=MAX0(M1/2,1)
      GO TO 21
20    MM=MM/2
      IF (MM .LE. 0) GO TO 100
21    K=N-MM
22    DO 1 J=1,K
        II=J
11    IM=II+MM
        IF (A(IM) .GE. A(II)) GO TO 1
        TEMP=A(II)
        IT=KEY(II)
        A(II)=A(IM)
        KEY(II)=KEY(IM)
        A(IM)=TEMP
        KEY(IM)=IT
        II=II-MM
        IF (II .GT. 0) GO TO 11
1     CONTINUE
      GO TO 20
100   RETURN
      END
```

\*\*\*\*\*  
\*  
\*\*\*\*\*

```
      SUBROUTINE VAR(Z, NUMZ, ZBAR, ZVAR)
C
C     << SUBROUTINE VAR WILL COMPUTE THE MEAN AND THE VARIANCE      >>
C     << OF ARRAY Z                                                  >>
C
      REAL Z(NUMZ), SUMZ, SUMZ2, ZBAR, ZVAR

      SUMZ = 0
      SUMZ2 = 0

      DO 100 I = 1, NUMZ

        SUMZ = SUMZ + Z(I)
```



```

      SUMZ2 = SUMZ2 + Z(I) ** 2
100 CONTINUE

      ZBAR = SUMZ / NUMZ
      ZVAR = ABS( SUMZ2 / NUMZ - ZBAR ** 2 )

      RETURN
      END

```

```

*****
*
*****

```

```

      SUBROUTINE FINDJ(A, R, J)
C
C      << SUBROUTINE FINDJ FINDS THE INDEX OF ARRAY A  WHICH THE      >>
C      << VALUE OF IT IS CLOSEST TO R.                                >>
C
      REAL A(1000), R, VALUE
      INTEGER J

      VALUE = ABS(A(1000) - R)

      DO 100 I = 999, 1, -1

        IF (ABS(A(I) - R) .LT. VALUE) THEN
          VALUE = ABS(A(I) - R)
        ELSE
          J = I + 1
          RETURN
        ENDIF
      100 CONTINUE

      RETURN
      END

```

```

*****
*
*****

```

```

      SUBROUTINE TNYVAL(R,SIGMAX,NUMX,ALPHA,ZALPHA,MUX,YO,
*          TBRL1,TCIR1)
C
C      << SUBROUTINE TNYVAL IS THE CASE WHEN X IS TRUNCATED NORMAL      >>
C      << AND Y IS GIVEN A VALUE                                         >>
C
      REAL R, SIGMAX, ALPHA, TALPHA, MUX, P(2), ZP(2), A(2)
      REAL X(100), X1, TEMP1, TEMP2, YO
      REAL TARL1(1000), KEY(1000), TRL1(1000), TBRL1(2), TCIR1(2)

      INTEGER NUMX, CASE, COUNT

```

```

DATA P / .95, .90 /
DATA ISEED, JSEED / 4875, 7981 /

DO 400 I = 1, 2

    P(I) = 1 - P(I)
    COUNT = 0

    CALL ZTABL2(P(I), ZP(I))

    A(I) = MUX + ZP(I) * SIGMAX

    DO 200 J = 1, 1000

100      CALL LNORM(ISEED, X1, 1, 2, 0)

        XTEMP = MUX + SIGMAX * X1

        IF (XTEMP .LE. A(I)) THEN
            COUNT = COUNT + 1
            X(COUNT) = XTEMP
        ELSE
            GOTO 100
        ENDIF

        IF (COUNT .LT. NUMX) GOTO 100

        CALL VAR(X, NUMX, XBAR, XVAR)

C          /* NOW WE COMPUTE THE LOWER CONFIDENCE BOUND */
          TEMP1 = (XBAR - Y0) / SQRT(XVAR*(NUMX-1) / NUMX)
          TEMP2 = 1. / NUMX +
*             ((XBAR - Y0) ** 2) / (2*(NUMX+1) * XVAR)
          TEMP1 = TEMP1 - ZALPHA * SQRT(TEMP2)

C          /* SUBROUTINE ZTABL1 COMPUTE RIGHT CUMULATIVE PROBABILITY FROM RIGHT PERCENT POINT. */
C          CALL ZTABL1(TEMP1, TARL1(J))

          TARL1(J) = 1. - TARL1(J)

200      CONTINUE

C          /* NON-IMSL LIBRARY 'SHSORT' WILL SORT TARL1 BY SHELL SORT ALGORITHM. */
C          CALL SHSORT(TARL1, KEY, 1000)

          DO 300 J = 1, 1000
              TARL1(J) = TARL1(J)

```

300 CONTINUE

```
C      /* SUBROUTINE FINDJ FINDS THE INDEX OF TARL1 WHICH THE      */
C      /* VALUE OF IT IS CLOSEST TO R.                          */
```

CALL FINDJ(TARL1, R, J)

```
C      /* DIVIDING THE INDEX BY 1000 WILL GIVE US TRUE          */
C      /* CONFIDENCE LEVEL.                                     */
```

TCIR1(I) = J / 1000.

MM = 1000 \* (1 - ALPHA)

TBRL1(I) = TRL1(MM)

400 CONTINUE

RETURN

END

```
*****
*
*****
```

SUBROUTINE JKNIFE(X, N, YO, ZHAT)

```
C
C      << THIS ROUTINE IS FOR THE 'JACKKNIFE' METHOD.          >>
C      << DUMMY PARAMETER IS ZHAT.                            >>
```

REAL X(N),XOMIT(100),XOMBAR(100),XOMVAR(100),ZOMHAT(100),ZHAT  
INTEGER M, N

M = N - 1

SUM = 0.

DO 200 I = 1, N  
DO 100 J = 1, M

```
IF (J .GE. I) THEN
XOMIT(J) = X(J+1)
ELSE
XOMIT(J) = X(J)
ENDIF
```

100 CONTINUE

CALL VAR(XOMIT, M, XOMBAR(I), XOMVAR(I))

ZOMHAT(I) = ( XOMBAR(I) - YO ) / SQRT(XOMVAR(I))  
SUM = SUM + ZOMHAT(I)

200 CONTINUE

ZHAT = SUM / N

RETURN  
END

## LIST OF REFERENCES

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